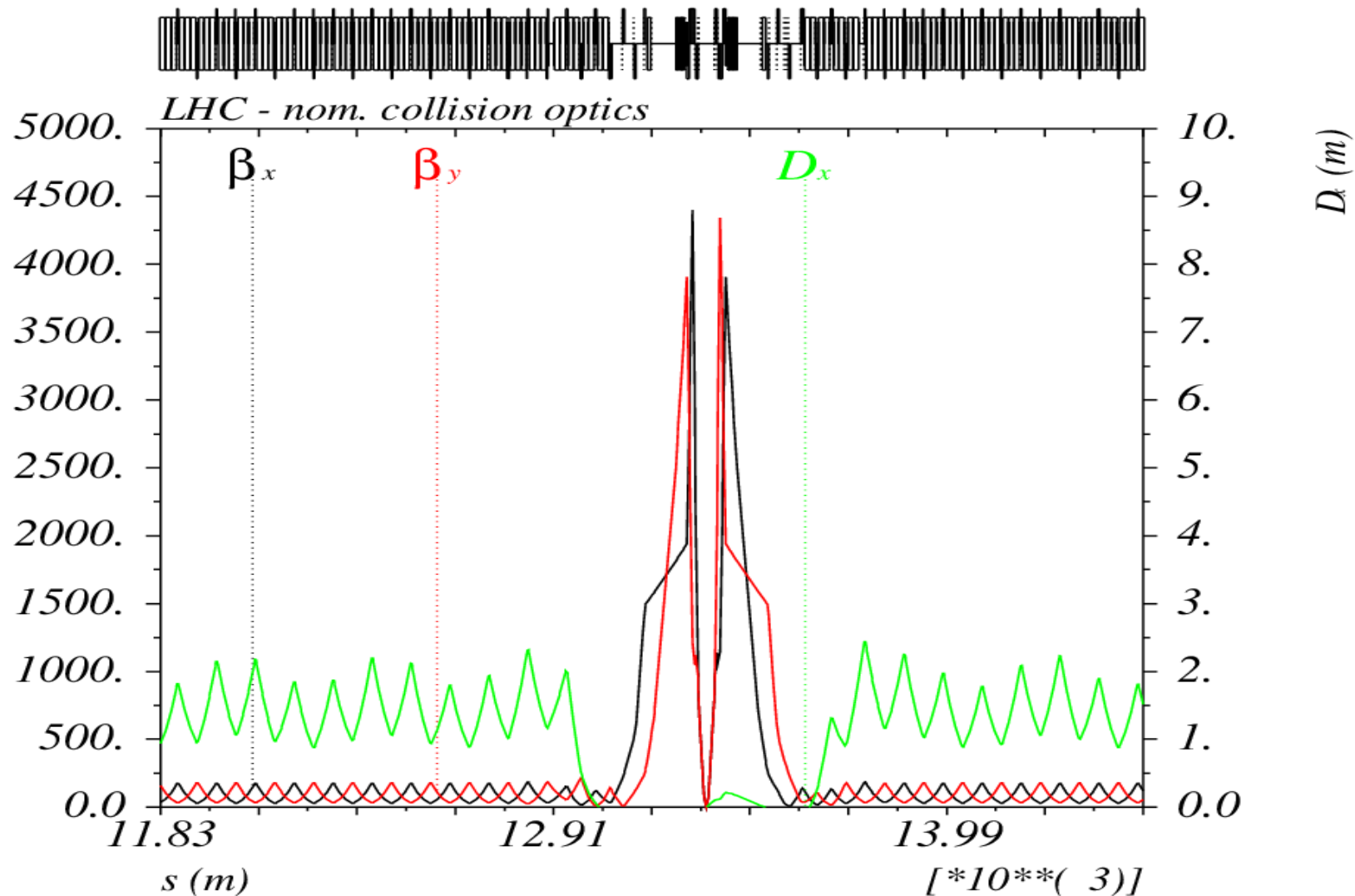


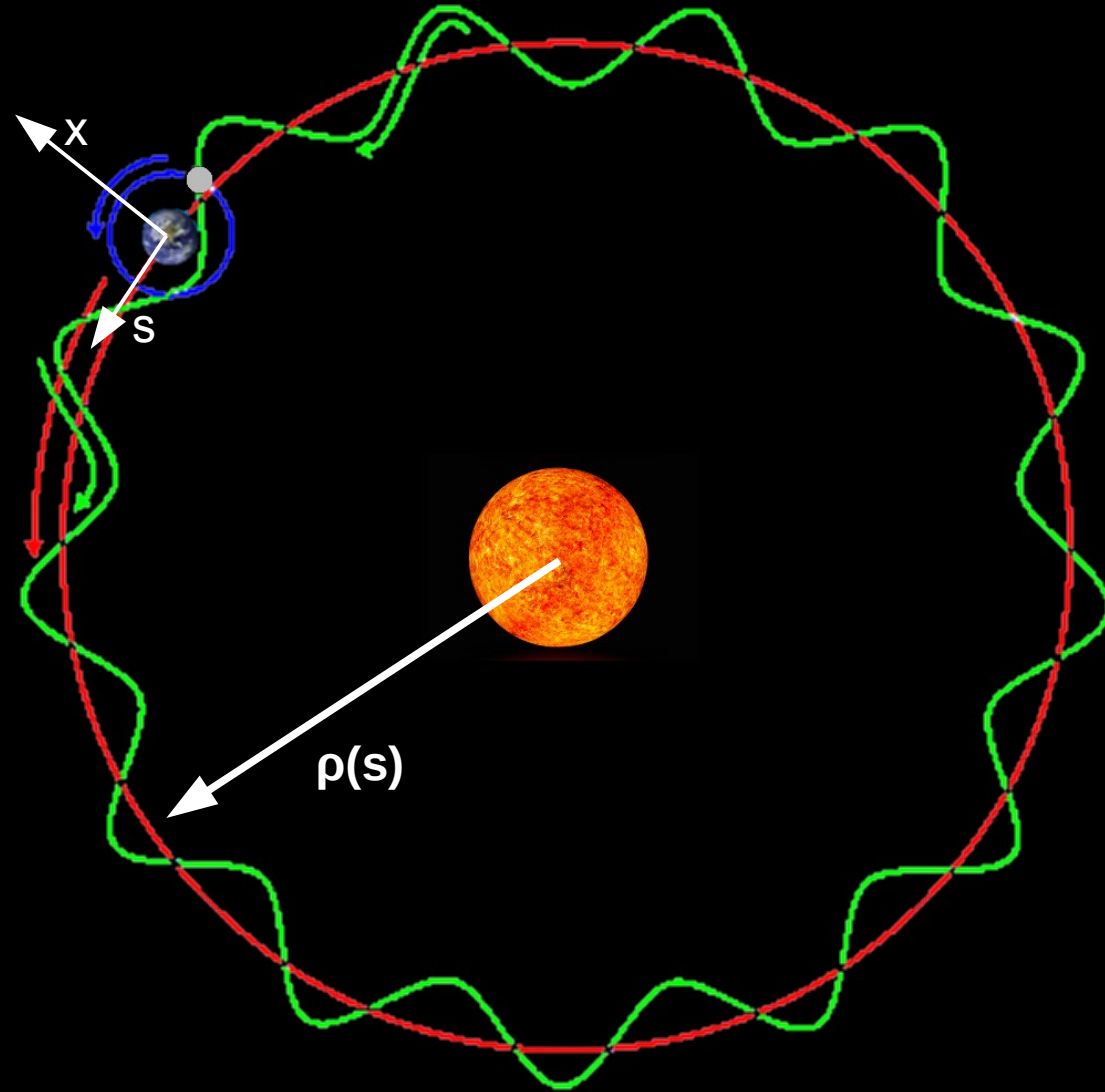
Accelerator Lattice Design – Part II Insertions

Ralph J. Steinhagen, CERN



- Acknowledgements and credits to: W. Herr, B. Holzer, A. Streun, A. Wolski

Moon's Trajectory around Sun



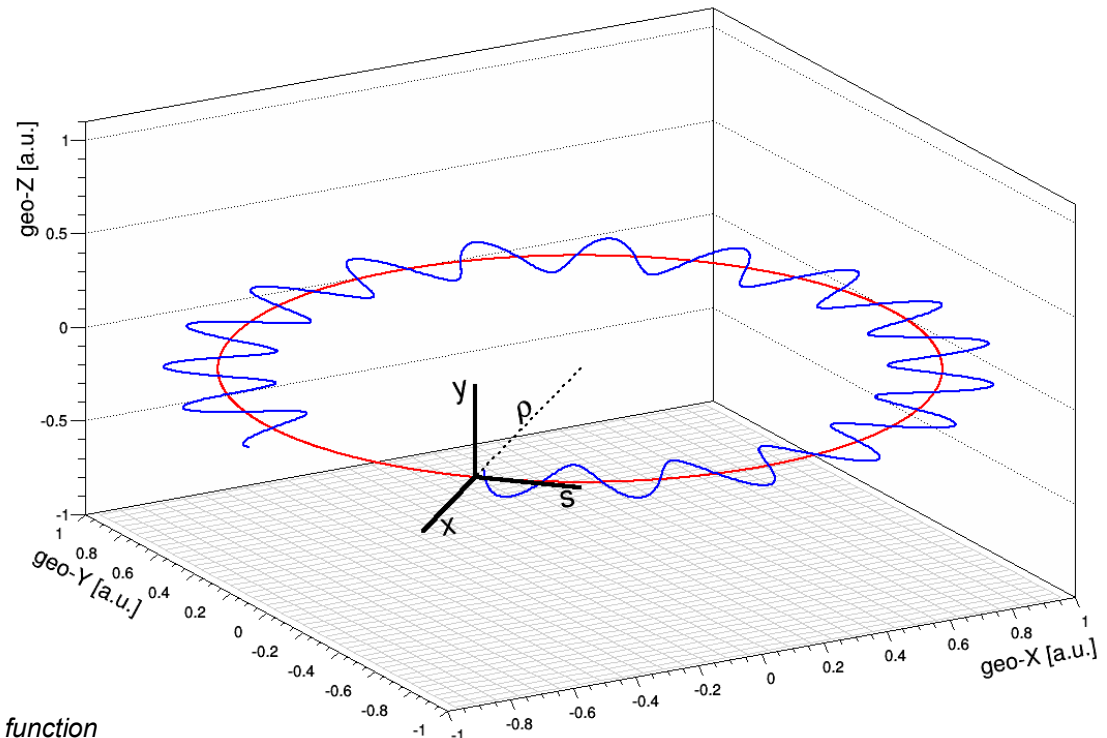
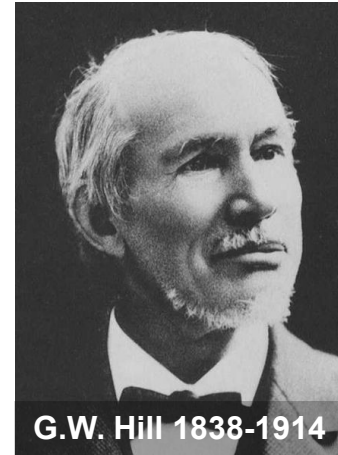
Recap: Transverse Beam Dynamics

- Hill's equation^{1,2}:

$$z'' + K(s) \cdot z = f(s, t)$$

$$K(s) = \underbrace{\frac{q}{p} B_{dipole}}_{\text{weak focusing: } \frac{1}{\rho}} - \underbrace{\frac{q}{p} \frac{\partial B_y}{\partial x}}_{\text{strong focusing: } k(s)}$$

- $k(s)$: focusing strength, defines:
 - betatron function $\beta(s)$ → envelope of the oscillation
 - dispersion function $D(s)$ → trajectory for off-momentum $\Delta p/p_0$ particles
- $f(s,t)$: external driving force



¹George William Hill, "On the part of the motion of the lunar perigee which is a function of the mean motions of the sun and moon", Acta Mathematica, 8:1–36, 1886

²coordinate 'z' being place holder for either x,y

Recap: Transverse Beam Dynamics

- Hill's equation for non-zero momentum spread $\Delta p/p_0$

$$z'' + K(s) \cdot z = \frac{\Delta p}{p_0} \cdot \frac{1}{\rho}$$

$$K(s) = \underbrace{\left(\frac{q}{p} B_{dipole} \right)^2}_{\text{weak focusing: } \frac{1}{\rho^2}} - \underbrace{\frac{q}{p} \frac{\partial B_y}{\partial x}}_{\text{strong focusing: } k(s)}$$

- General Solution

$$z(s) = \underbrace{z_{co}(s)}_{\text{closed orbit}} + \underbrace{D(s) \cdot \frac{\Delta p}{p_0}}_{\text{dispersion orbit}} + \underbrace{z_{\beta}(s)}_{\text{betatron oscillations}}$$

- Propagation through the ring:

$$D(s) = \underbrace{m_{12}(s)}_{\sim \cos(\mu)} \oint \frac{1}{\rho(\tilde{s})} m_{11}(\tilde{s}) d\tilde{s} - \underbrace{m_{21}(s)}_{\sim \sin(\mu)} \oint \frac{1}{\rho(\tilde{s})} m_{12}(\tilde{s}) d\tilde{s}$$

- Two important take-away messages:

- weak dipoles \rightarrow large bending radius \rightarrow small dispersion
- Drifts or quadrupoles: $1/\rho = 0$

Recap: Transverse Beam Dynamics

- Defines add. 'Twiss' functions¹: betatron phase advance $\mu(s)$, $\alpha(s)$ & $\gamma(s)$

$$\Delta \mu(s) := \int_0^s \frac{1}{\beta(s')} ds' \quad \alpha(s) := -\frac{\beta'(s)}{2} \quad \gamma(s) := \frac{1 + \alpha^2(s)}{\beta(s)}$$

- First-order solution to Hill's equation:

$$z(s) = \underbrace{z_{co}(s)}_{\text{closed orbit}} + \underbrace{D(s) \cdot \frac{\Delta p}{p_0}}_{\text{dispersion orbit}} + \underbrace{z_{\beta}(s)}_{\text{betatron oscillations}}$$

→ sinusoidal particle motion in accelerators:

$$z_{\beta}(s) = \sqrt{\epsilon_i \beta(s)} \cdot \sin(\mu(s) + \phi_i)$$

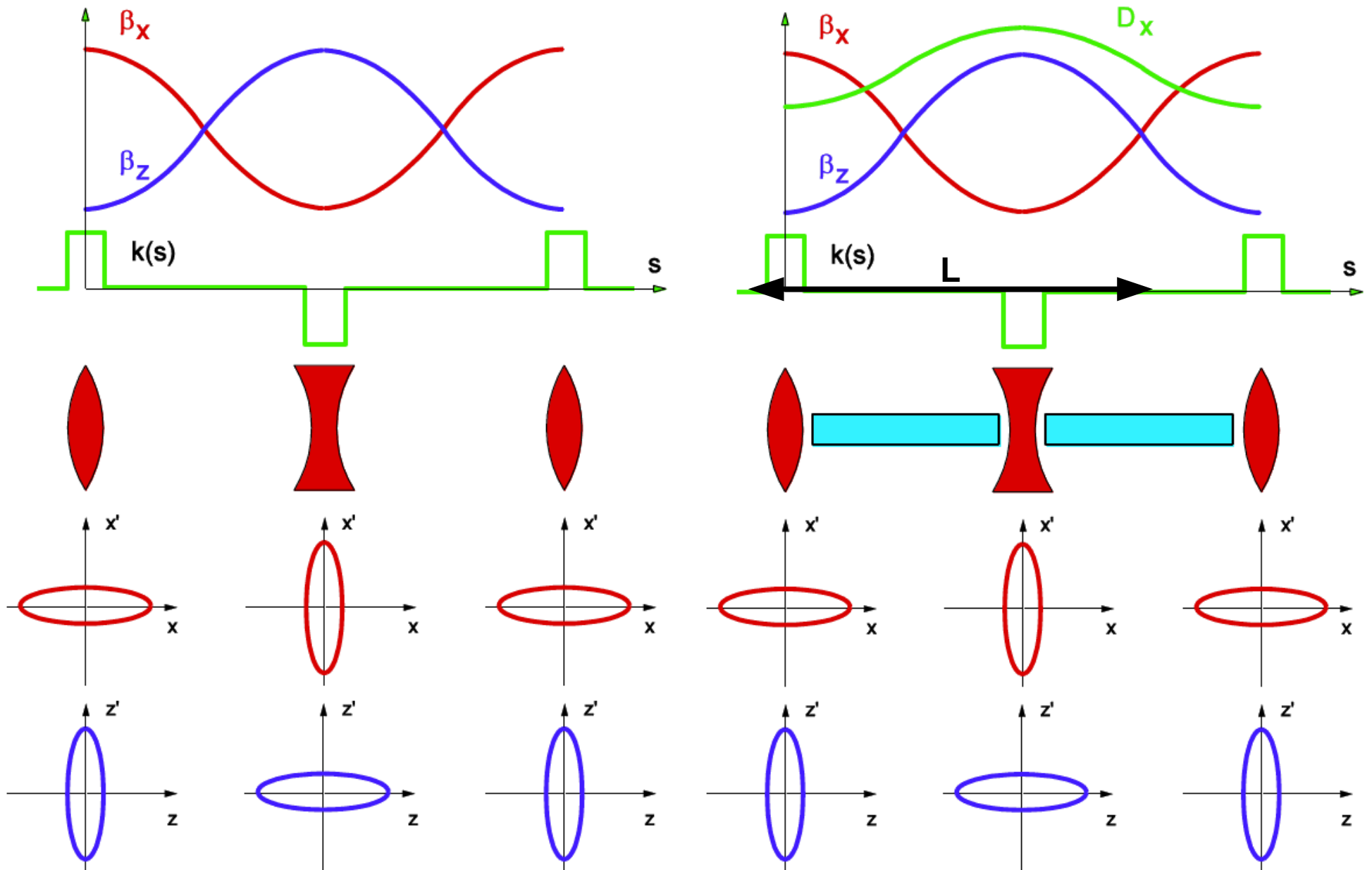
ϵ_i, ϕ_i : initial particle state

- Courant-Snyder invariant of motion (\leftrightarrow energy conservation)

$$\epsilon = \beta(s) \cdot x'^2 + 2\alpha(s) \cdot x x' + \gamma(s) \cdot x^2$$

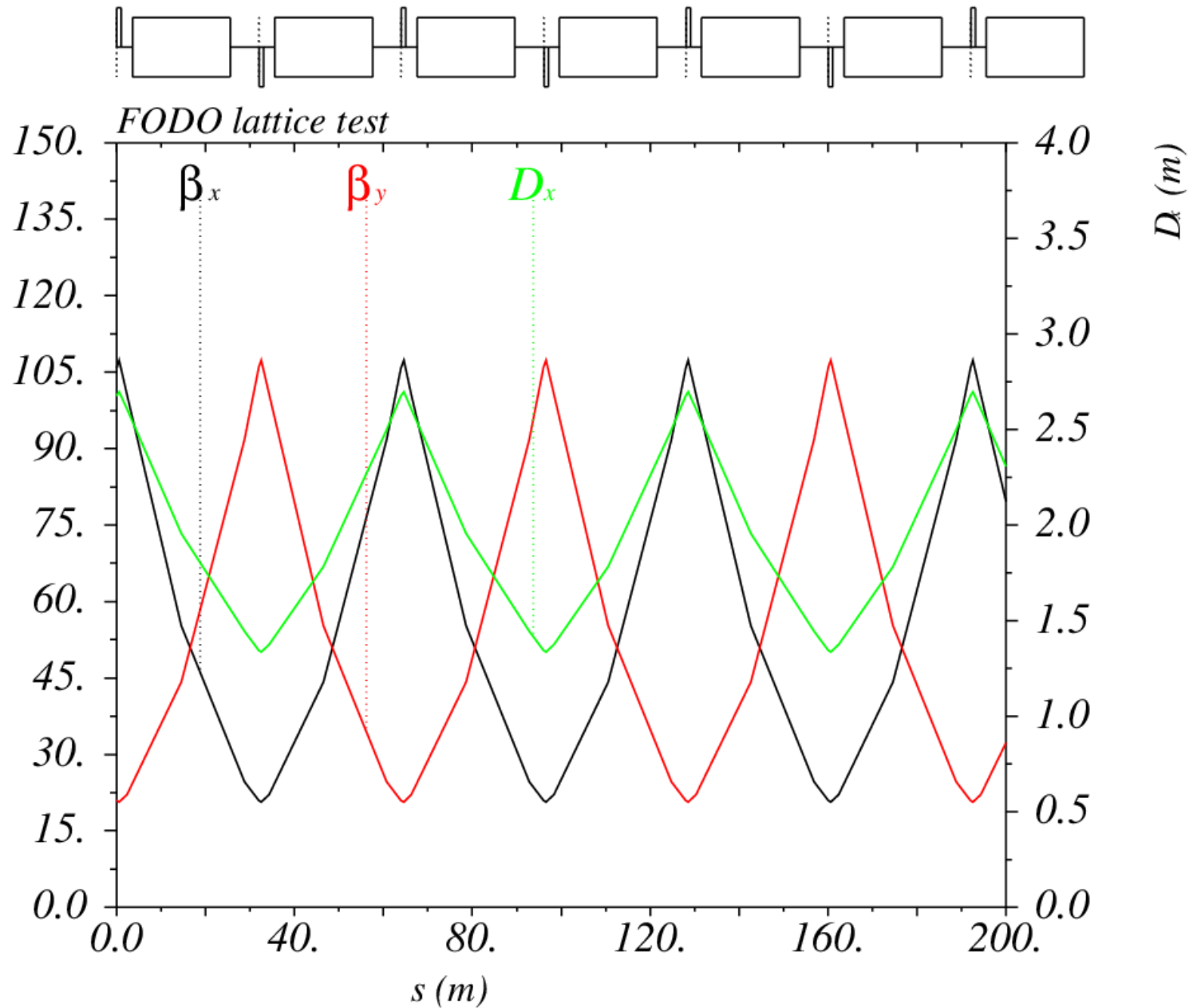
¹Richard Q. Twiss and N. H. Frank, "Orbital stability in a proton synchrotron", Rev. Sci. Instr., 20(1):1–17, January 1949.

Recap: FoDo Lattice



Courtesy L. Rivkin, EPFL & PSI

Recap: FoDo Lattice



Recap: FoDo Lattice – Summary

- FoDo cell transfer matrix (→ tutorial)

$$M_{FoDo} = \begin{pmatrix} 1 - \frac{L^2}{2f^2} & L \left(1 + \frac{L}{2f} \right) \\ \left(\frac{L^2}{2f^3} - \frac{L}{f^2} \right) & 1 - \frac{L^2}{2f^2} \end{pmatrix}$$

- Phase advance per cell (→ tutorial)
 - N.B. also correct for non-FoDo cells

$$\cos \mu_{cell} = \frac{1}{2} \text{trace}(M)$$

- Equations guide 1st-order cell design
→ input for non-linear numerical optimisations (tutorial)

$$\begin{aligned} f &= \pm \frac{L}{4 \sin \frac{\mu}{2}} = (kl_q)^{-1} \\ \beta^\pm &= \frac{L(1 \pm \sin \frac{\mu}{2})}{\sin \frac{\mu}{2}} \\ \alpha^\pm &= \frac{\mp 1 - \sin \frac{\mu}{2}}{\cos \frac{\mu}{2}} \\ D^\pm &= \frac{L \varphi \left(1 \pm \frac{1}{2} \sin \frac{\mu}{2} \right)}{4 \sin^2 \frac{\mu}{2}} \\ \xi_{FODO} &= -\frac{1}{\pi} \tan \frac{\mu}{2} \end{aligned}$$

Overview

- Part I – we learned ...
 - ... how to design simple FoDo lattice,
 - ... how to compute optical functions,
 - ... to match simple global parameters (tune, chromaticity),
 - ... and did some simple particle tracking.

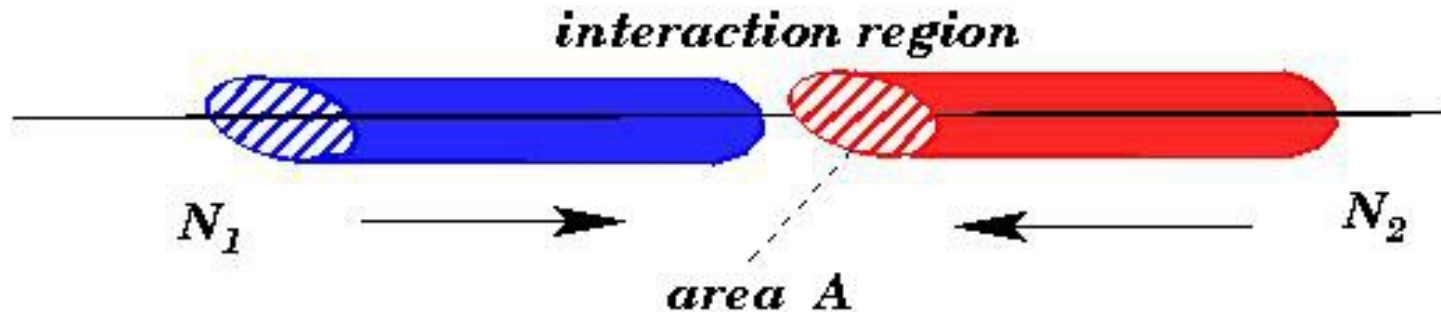
- Part II
 - Machines with imperfections and corrections (dispersion)
 - Design of insertions
 - Dispersion suppressor
 - Low- β insertion

Matching Local Optical Parameters

- To get the optical configuration you want matching
 - Main applications:
 - Setting global optical parameters
 - Tune and chromaticity
 - Setting local optical parameters
 - Low (or high) β insertions
 - Dispersion suppressors
 - Correction of imperfections
- Adjust strength of individual machine elements

Luminosity: $dN_{\text{event}}/dt = L \sigma_{\text{process}}$

- Collider design:



$$L_{\text{peak}} \approx \frac{f_{\text{rev}} k_b \cdot N_b^2}{4\pi \sigma_x \sigma_y} \cdot F = \frac{f_{\text{rev}} \gamma k_b \cdot N_b^2}{4\pi \beta^* \epsilon_n} \cdot F$$

- N_b : number of particles per bunch,
- k_b : total number of bunches,
- σ_x, σ_y : hor./vert. r.m.s. beam size in IR,
- f_{rev} : revolution or repetition frequency,
- $F_{\text{corr.}}$: numerical correction factors (hour-glass, crossing angle, ...),
- ϵ : emittance (invariant of motion, ~"temperature of bunch")

$$\sigma_{x,y} = \sqrt{\frac{\epsilon^* \beta(s)}{\gamma} + \dots}$$

Most Simple Example – Drift Space I/II

$$M_{drift} = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} = \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix}$$

- Particle coordinates:

$$\begin{pmatrix} x \\ x' \end{pmatrix} = \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}_0$$

$$\begin{aligned} x(L) &= x_0 + L \cdot x'_0 \\ x'(L) &= x'_0 \end{aligned}$$

- Transformation of Twiss parameters

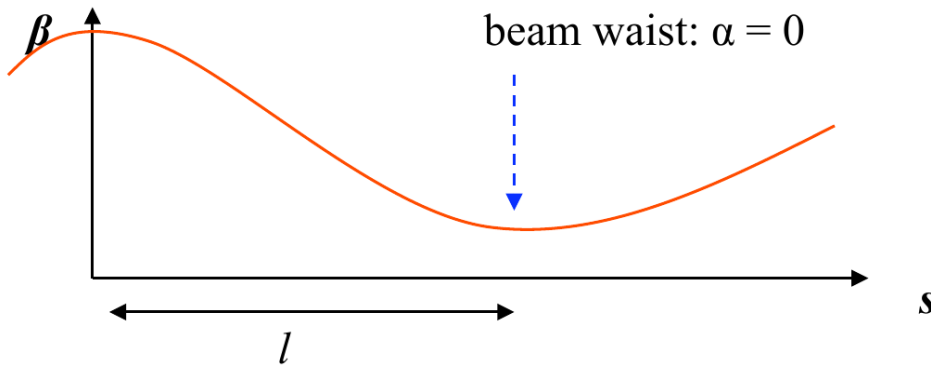
$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix} = \begin{pmatrix} 1 & -2L & L^2 \\ 0 & 1 & -L \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0$$

$$\beta(s) = \beta_0 - 2\alpha_0 \cdot L + \gamma_0 \cdot L^2$$

$$\alpha(s) = \alpha_0 - L \cdot \gamma_0$$

→ equation being important for low-beta insertions

Most Simple Example – Drift Space II/II



$$(I) \quad \beta(s) = \beta_0 - 2\alpha_0 \cdot L + \gamma_0 \cdot L^2$$

$$(II) \quad \alpha(s) = \alpha_0 - L \cdot \gamma_0$$

- Beam size is smallest at $\alpha(s) = 0 \rightarrow \alpha_0 = \gamma_0 \cdot s$

$$\rightarrow L = \alpha_0 / \gamma_0$$

- Beam size at that point: $\gamma(L) = \gamma_0$ & $\alpha(L) = 0$

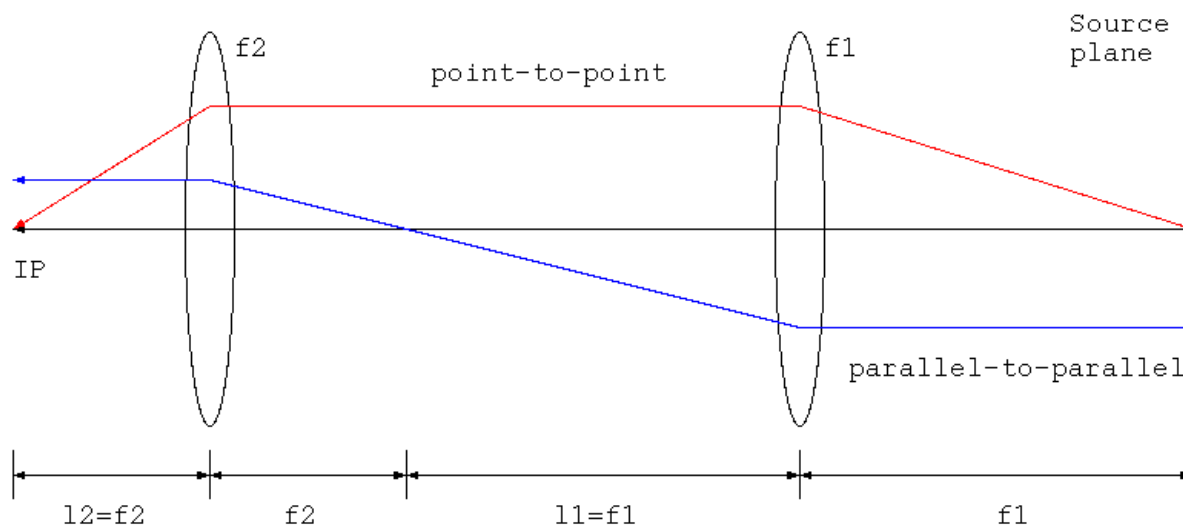
$$\rightarrow \beta(L) = 1 / \gamma_0$$

- Inserting in (I):

$$\beta(s) = \beta_0 + \frac{s^2}{\beta_0}$$

- Phase advance: $\Delta\mu(s) := \int_{-L}^{+L} \frac{1}{\beta(s')} ds' \approx \pi$

Telescope and low β



- Doublet or Triplet
- Point-to-point $R_{12}=0$
- Parallel to parallel $R_{21}=0$
- R_{11} =demagnification
- Ratio of focal lengths
- Needs to work in both planes with doublets/triplets

$$\begin{pmatrix} 1 & l_1 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -1/f_1 & 1 \end{pmatrix} \begin{pmatrix} 1 & l_1 \\ 0 & 1 \end{pmatrix} = \begin{pmatrix} 1 - l_1/f_1 & 2l_1 - l_1^2/f_1 \\ -1/f_1 & 1 - l_1/f_1 \end{pmatrix}$$

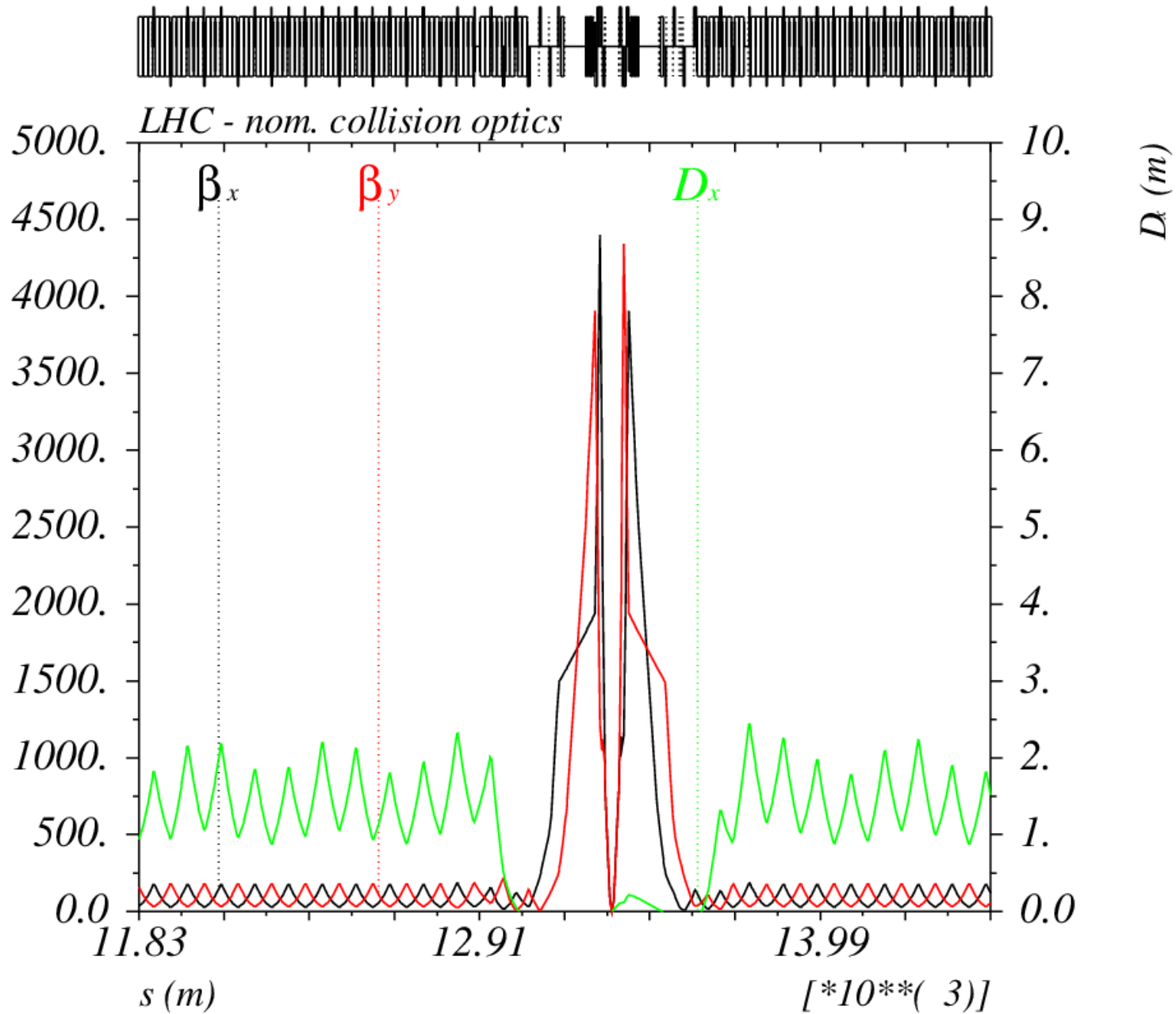
For one module with $l_1 = f_1$

$$\begin{pmatrix} 0 & f_1 \\ -1/f_1 & 0 \end{pmatrix}$$

For both modules:

$$R = \begin{pmatrix} -f_2/f_1 & 0 \\ 0 & -f_1/f_2 \end{pmatrix}$$

Example LHC



LHC: Squeezing in ATLAS – Beam Envelope

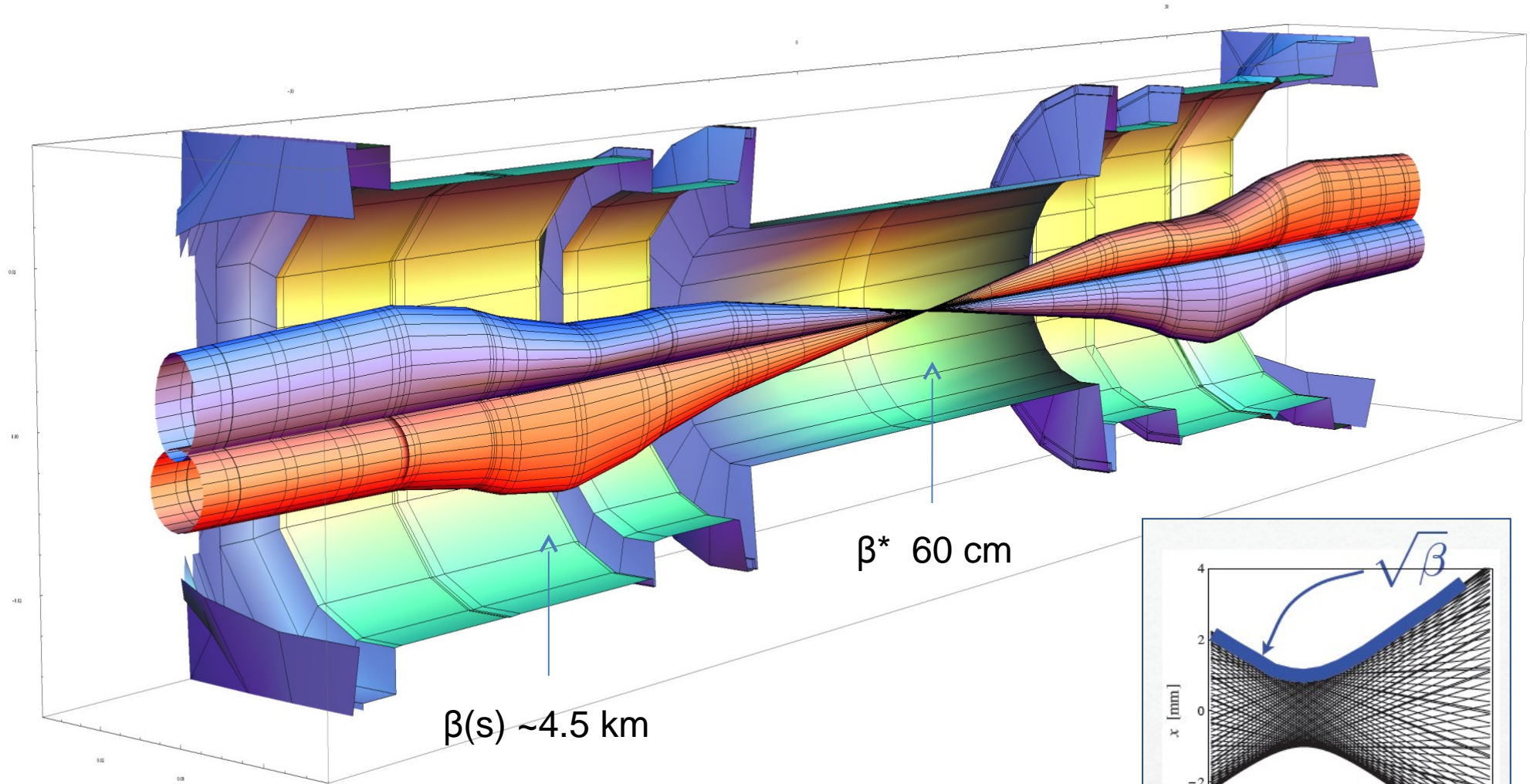
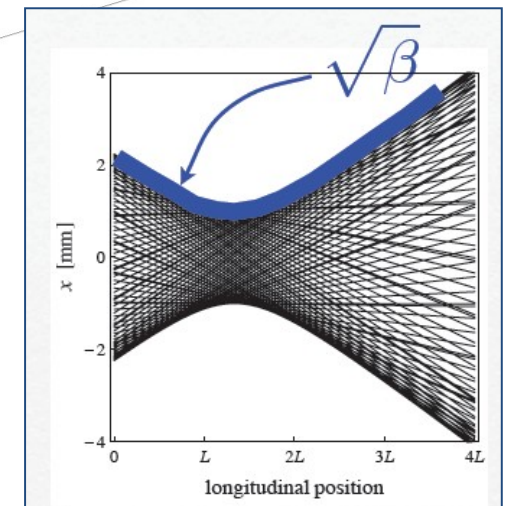
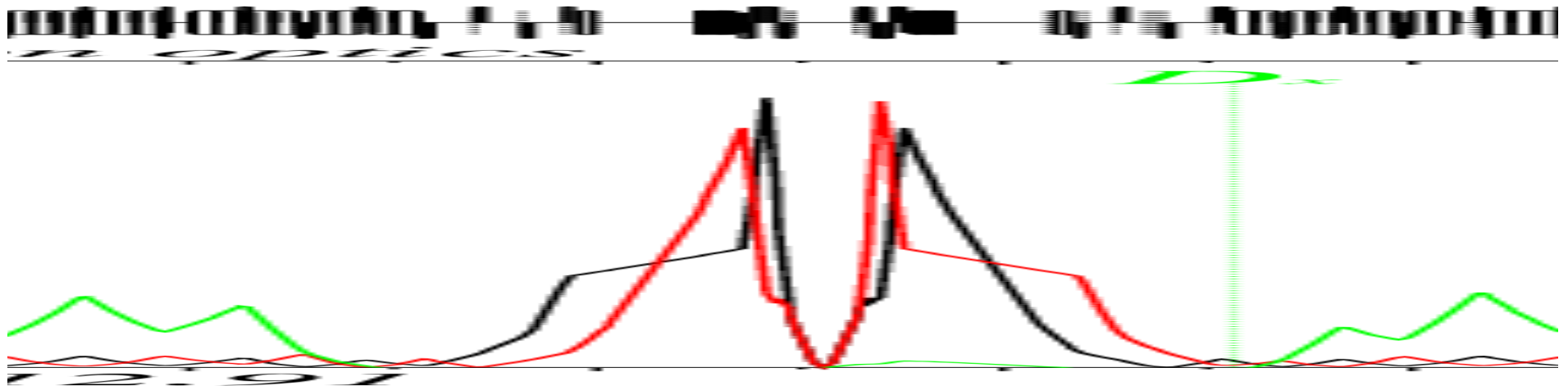


Image courtesy John Jöwett



Low β : Design Guidelines

1. Calculate the periodic solution in the arc (e.g. FODO)
 2. Insert the drift space for the insertion devices (e.g. undulator/detector)
 3. Put a quadrupole doublet (or: triplet) as close as possible
 4. Introduce additional quadrupole lenses to match the beam parameters to the values at the beginning of the arc structure
- Parameters to be optimised and matched to the periodic solution:
 - $\beta_x, \alpha_x, D_x, \beta_y, \alpha_y, D_y, Q_x, Q_y \rightarrow$ requires (at least) 8 independent quadrupoles



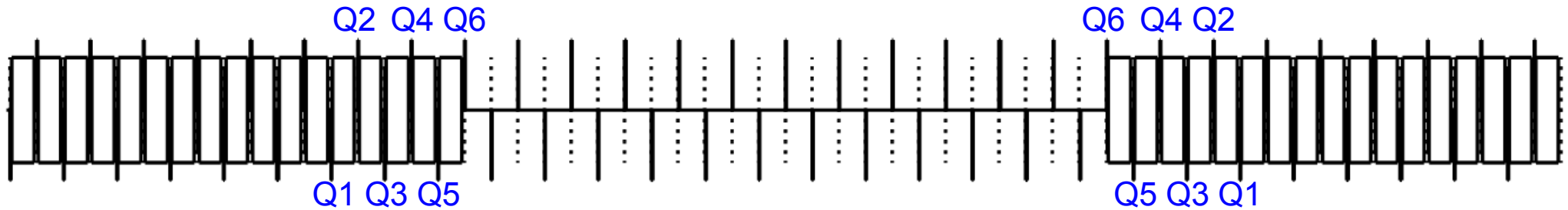
Dispersion Suppressors

- Beam size:

$$\sigma(s) = \sqrt{\epsilon \cdot \beta(s) + \left(D(s) \cdot \frac{\Delta p}{p_0} \right)^2}$$

- for small emittances dominated by dispersion
- need small sizes? → small dispersion!
 - for electron machines this is notably in the vertical plane
 - N.B. off-centre beam in quadrupoles → dipole kick → dispersion
- Various dispersion Suppressor schemes
 - “Full-Match”
 - “Missing-bend”
 - “Half-bend”

Dispersion Suppressor – Quadrupole Match I/II



- Idea: use 6 additional independent quadrupoles
 - Dispersion suppressed by two quadrupoles
 - β and α restored to the values of the periodic solutions by 4 additional quads

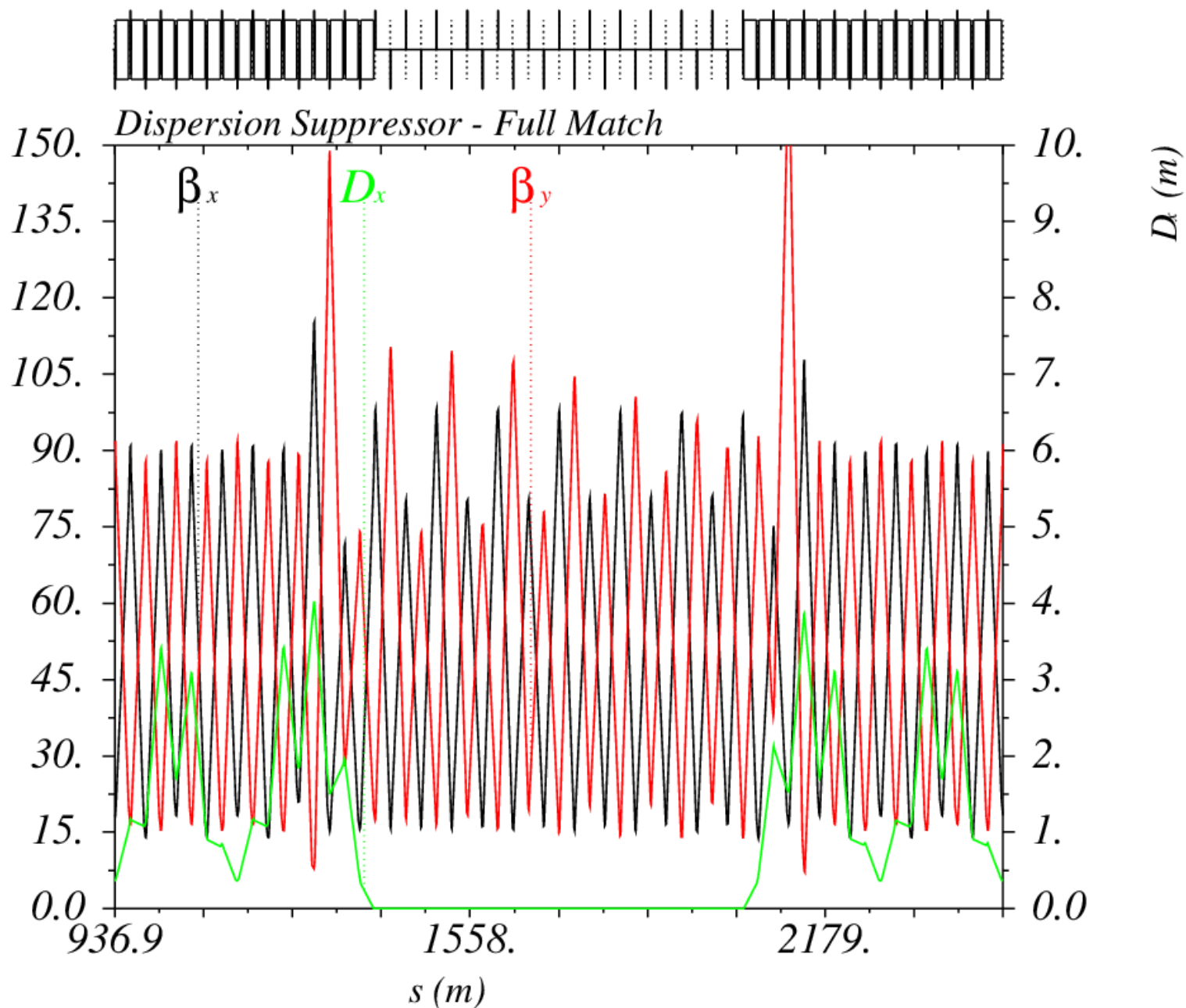
Advantage:

- Easy
- works for any phase-advance per cell
- Does not change the geometry of the storage ring
- Can be used to match between different lattice structures

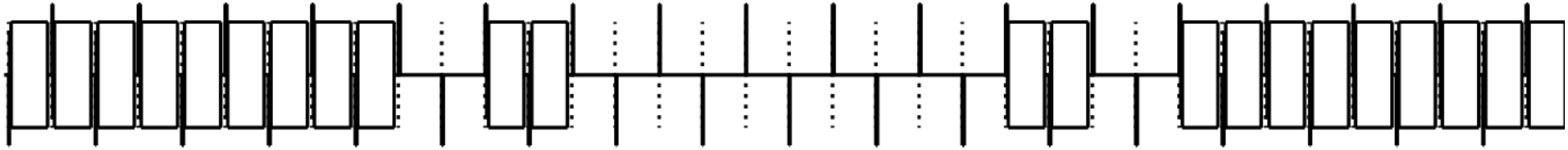
Disadvantage:

- additional power supplies needed (costs!)
- Requires stronger quadrupoles
- Due to higher- β values: more aperture needed

Dispersion Suppressor – Quadrupole Match II/II



Dispersion Suppressor – Missing Bend I/II



- Idea: create dispersion wave matching conditions at the first quadrupole

$$\frac{2m+n}{2} \Phi_c = (2k+1) \frac{\pi}{2}$$

- m = # of cells without dipoles, followed by n regular arc cells, Φ_c : cell phase-advance

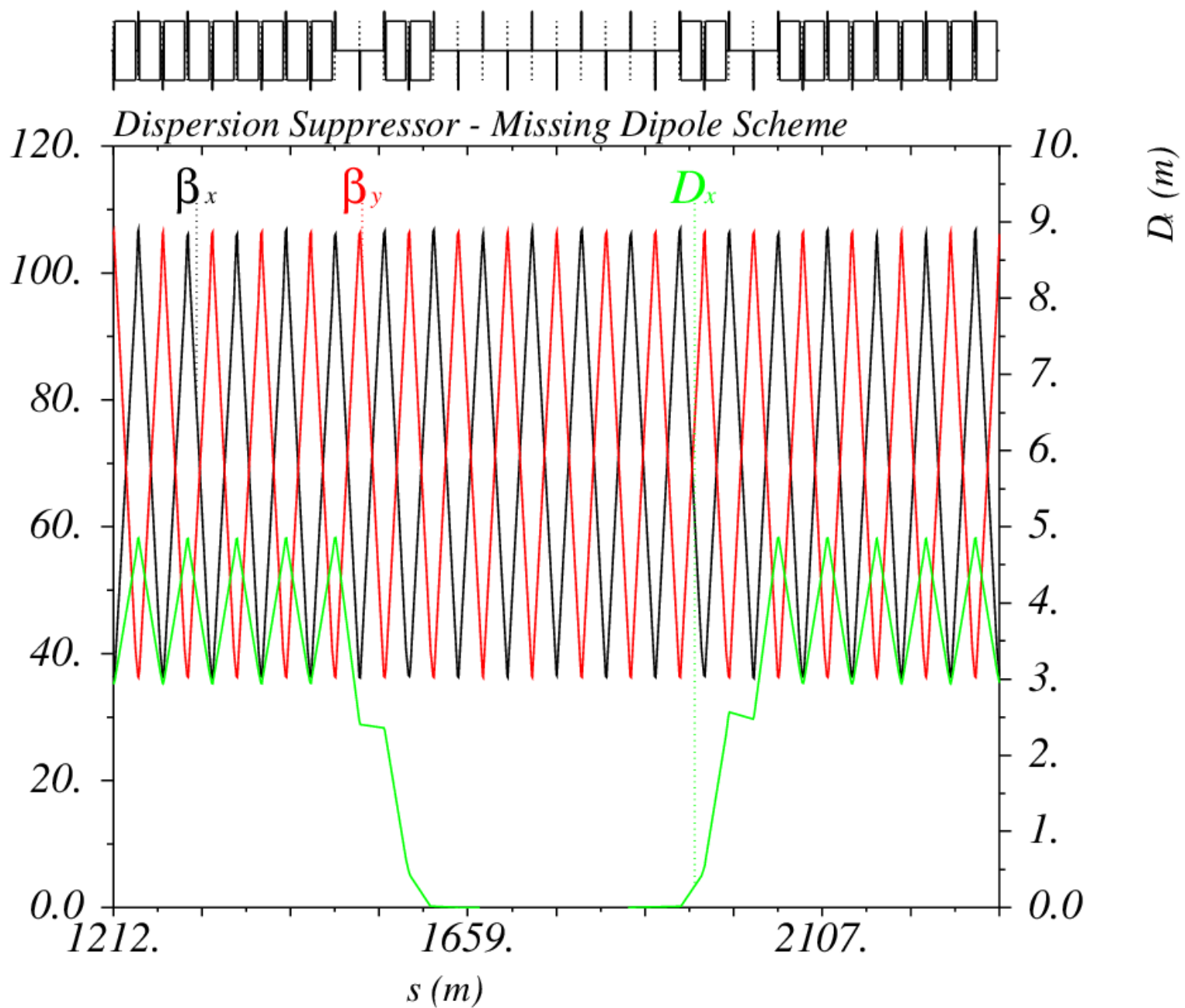
Advantage:

- Cost-effective
- Keeps the geometry of the arc cells

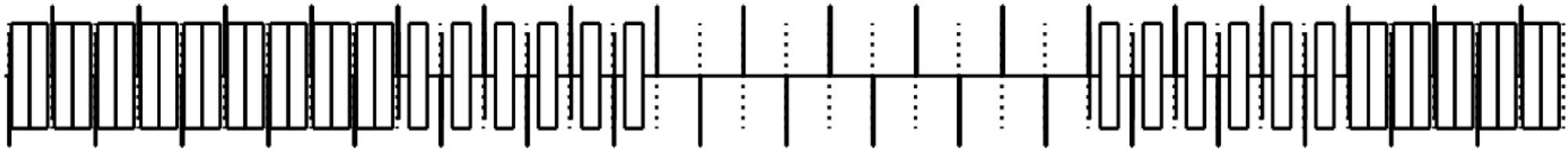
Disadvantage:

- In its simplest form constraints possible cell phase-advances Φ_c

Dispersion Suppressor – Missing Bend II/II



Dispersion Suppressor – Half-Bend I/II



- Idea: condition for vanishing dispersion

$$2 * \delta_{\text{supr}} * \sin^2\left(\frac{n\Phi_c}{2}\right) = \delta_{\text{arc}}$$

$$\delta_{\text{supr}} = \frac{1}{2} * \delta_{\text{arc}}$$

$$\sin(n\Phi_c) = 0$$

- $n = \#$ of cells with half-strength dipoles, Φ_c : cell phase-advance

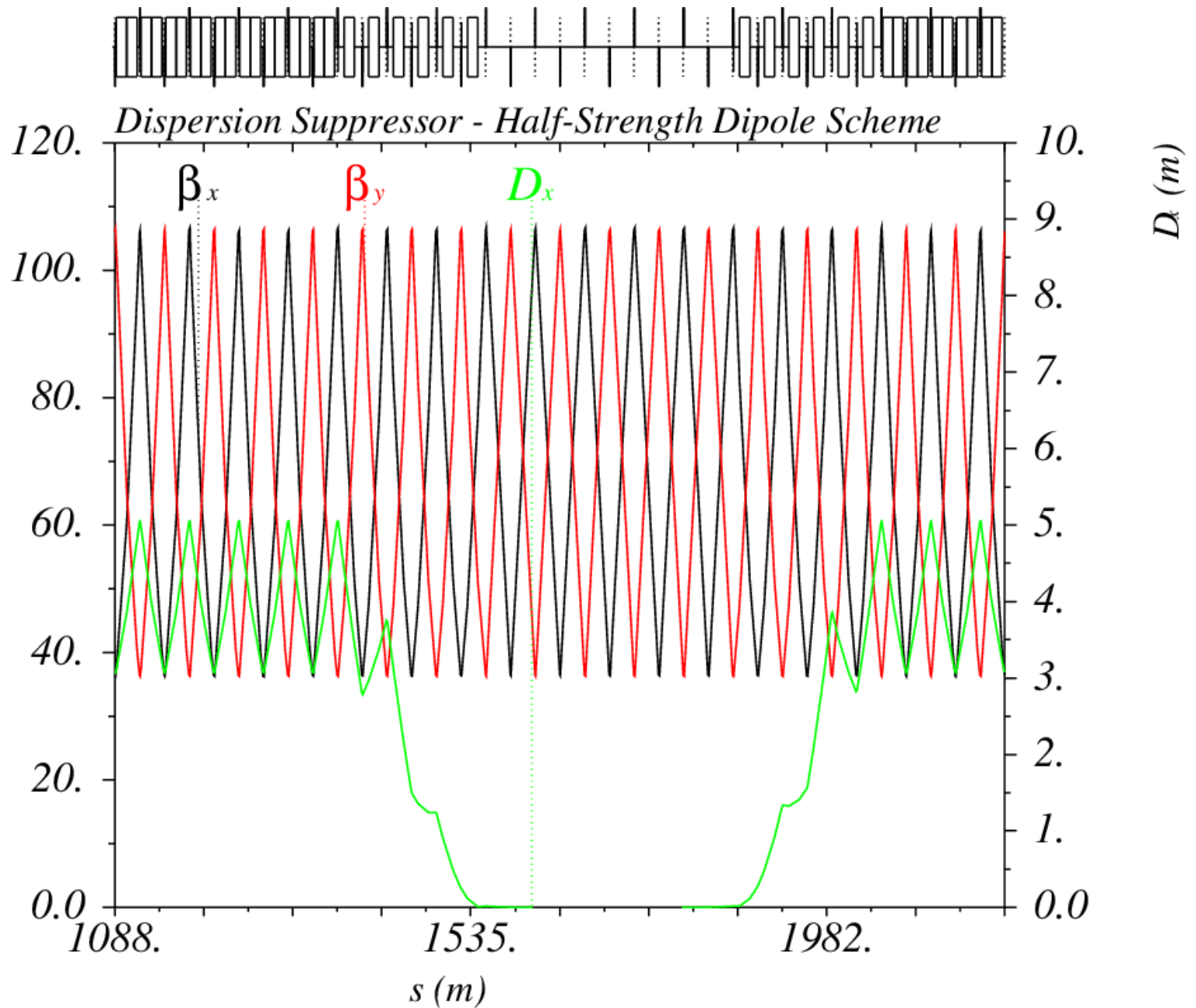
Advantage:

- Cost-effective
- Keeps the geometry of the arc cells

Disadvantage:

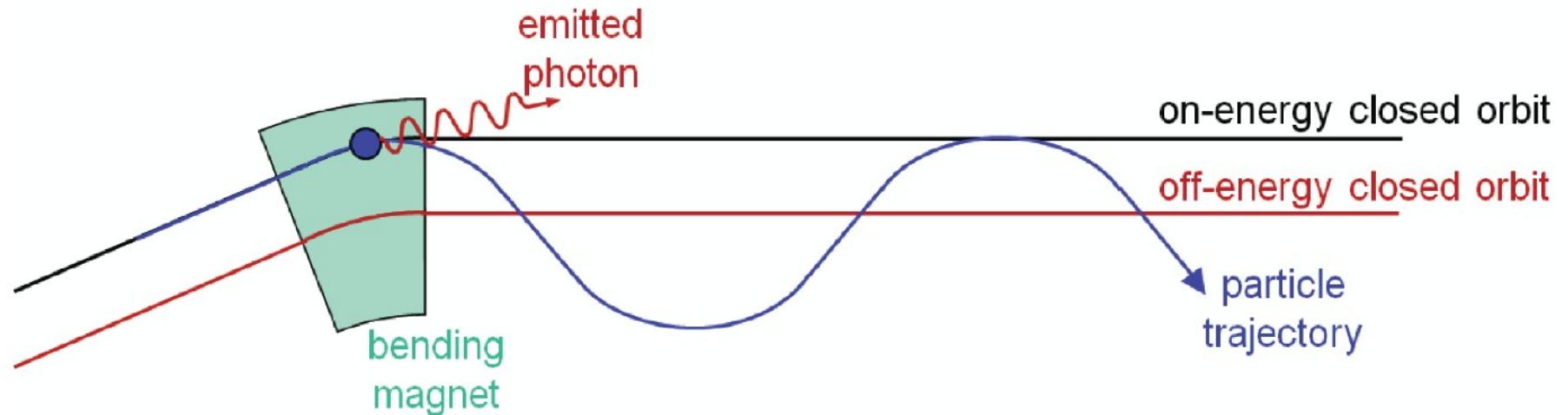
- In its simplest form constraints possible cell phase-advances Φ_c

Dispersion Suppressor – Half-Bend II/II



Natural Emittance

- Quantum nature of synchrotron radiation emission
→ finite electron beam size, emittance and energy spread



- oscillation damping and excitation counterbalance

$$\frac{d\varepsilon}{dt} = \frac{\gamma D^2 + 2\alpha D D' + \beta D'^2}{T} \delta_{rms}^2$$

Radiation Integrals

$$I_1 = \oint \frac{D_x}{\rho} ds, \quad \alpha_p = \frac{I_1}{C_0}$$

$$I_2 = \oint \frac{1}{\rho^2} ds,$$

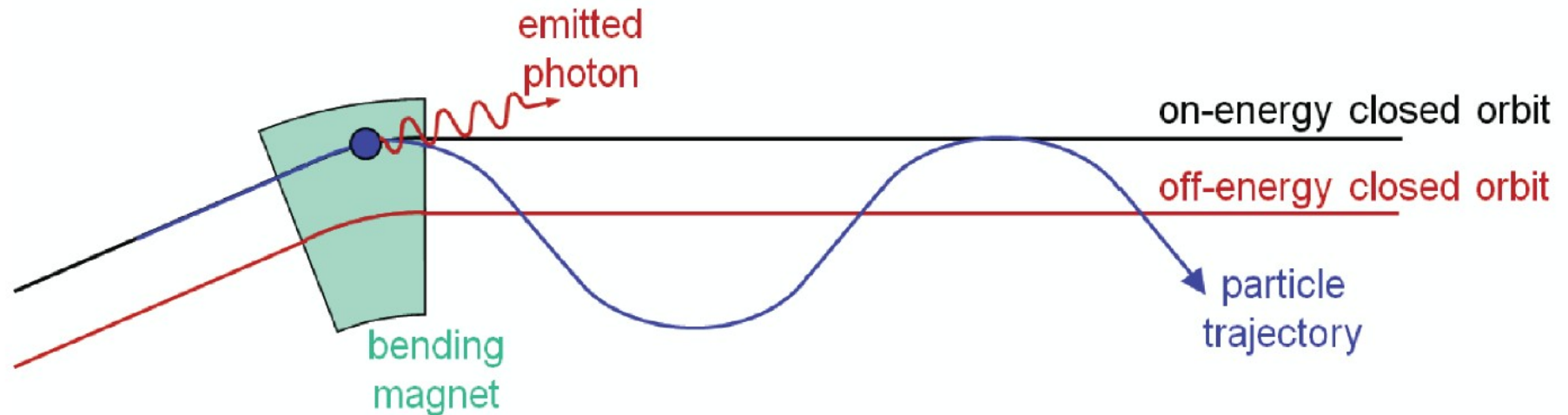
$$I_3 = \oint \frac{1}{|\rho^3|} ds,$$

$$I_4 = \oint \frac{D_x}{\rho} \left(\frac{1}{\rho^2} + 2k_1 \right) ds, \quad \text{with: } k_1 = \frac{q}{p_0} \frac{\partial B_y}{\partial x}$$

$$I_5 = \oint \frac{H_x}{|\rho^3|} ds, \quad \text{with: } H_x = \gamma_x D_x^2 + 2\alpha_x D_x D' + \beta D'^2$$

Natural Emittance

- Quantum nature of synchrotron radiation emission
→ finite electron beam size, emittance and energy spread



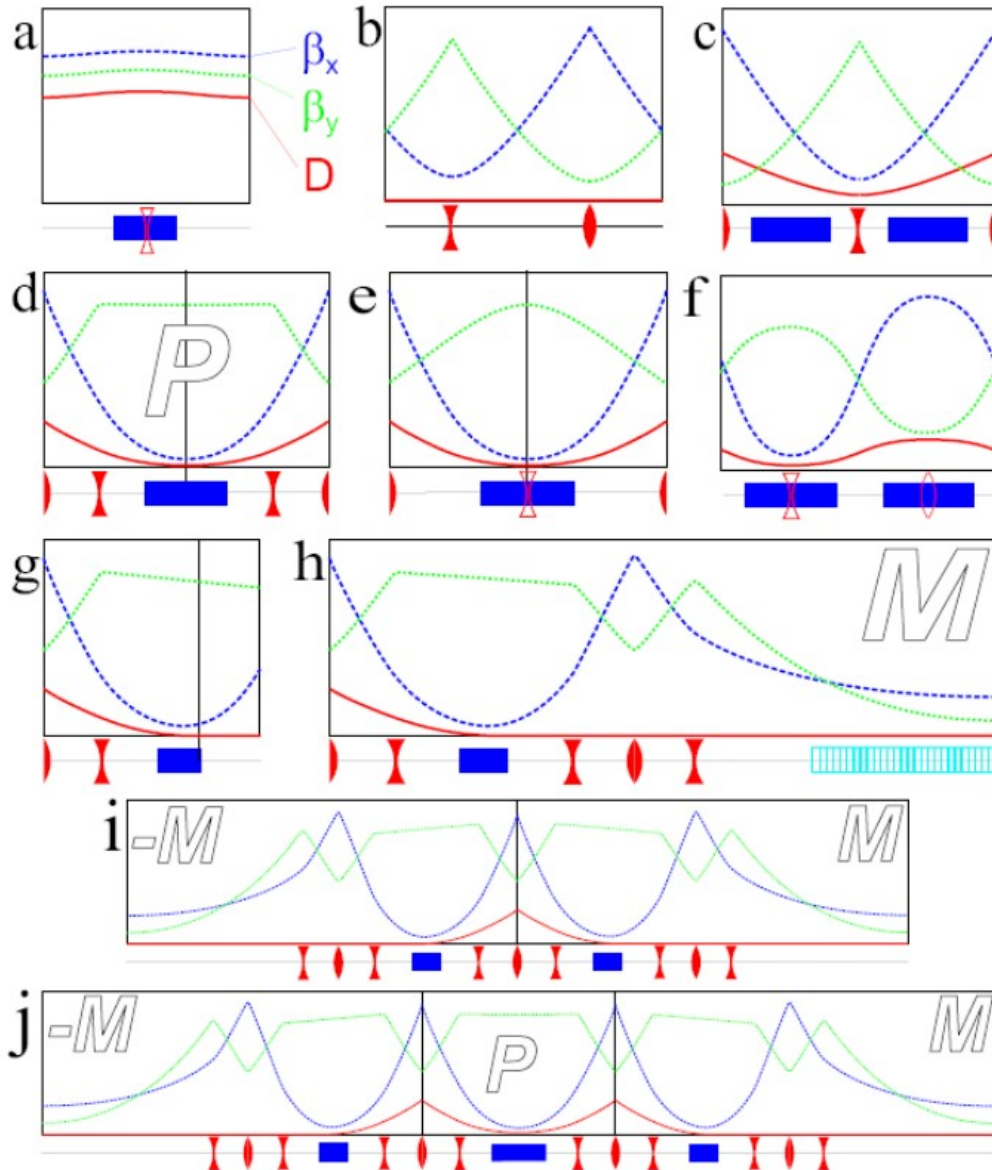
- damping and excitation counterbalance → equilibrium emittance:

$$\epsilon_0 = C_q \gamma^2 \frac{I_5}{j_x I_2}, \quad j_x = \underbrace{1 - \frac{I_4}{I_2}}_{\approx 1}, \quad \text{and} \quad C_q = \frac{55}{32\sqrt{3}} \frac{\hbar}{mc} \approx 3.832 \cdot 10^{-13} m$$

$$I_2 = \oint \frac{1}{\rho^2} ds,$$

$$I_5 = \oint \frac{H_x}{|\rho^3|} ds, \quad \text{with: } H_x = \gamma_x D_x^2 + 2\alpha_x D_x D'_x + \beta_x D'^2_x$$

Many Alternatives – Give it a try!



- a) Weak focusing (dipole only)
- b) FODO line (w/o dipoles)
- c) FODO cell
- d) Low-emittance cell
- e) CF low-emittance cell
- f) Low-emittance FODO
- g) Dispersion match
- h) Periodic dispersion match
- i) Double-bend achromat
- j) Triple-bend achromat
- k) ...

Very good course on low-emittance lattice design: A.Streun, PSI

Natural Emittance – A bit more Detail

$$\epsilon_0 \approx C_q \gamma^2 \frac{I_5}{j_x I_2}, \quad I_2 = \oint \underbrace{\frac{1}{\rho^2}}_{\sim \langle D \rangle_{ring}} ds, \quad I_5 = \oint \frac{H_x}{|\rho^3|} ds, \quad \text{with: } H_x = \gamma_x D_x^2 + 2\alpha_x D_x D' + \beta D'^2$$

- Important take-aways:

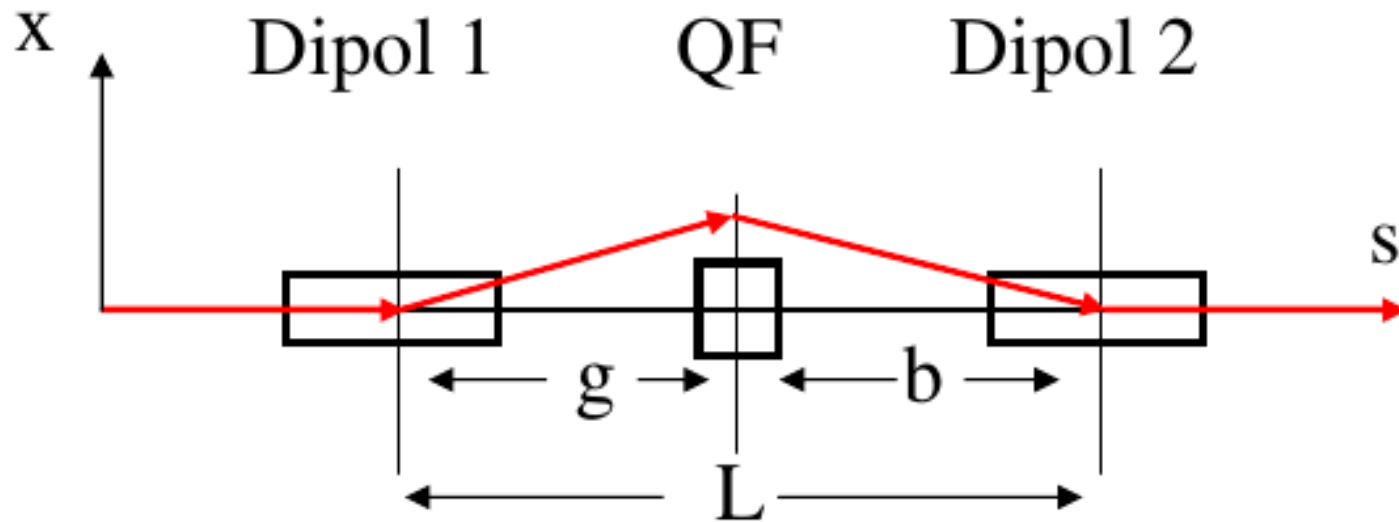
- minimise dispersion $D_x(s)$
- minimise deflection angle $|1/\rho^3| \sim \theta^3$
- arrange your dipoles and quadrupoles wisely

- Examples:

- FoDo $\epsilon_{0|min} \approx (2\sqrt{2} \dots 1.2) C_q \gamma^2 \theta^3,$
- DBA $\epsilon_{0|min} \approx \frac{1}{4\sqrt{14}} C_q \gamma^2 \theta^3,$
- TME $\epsilon_{0|min} \approx \frac{1}{12\sqrt{15}} C_q \gamma^2 \theta^3,$

Chasman-Green Double-Bend Achromat I/II

- Remember trick from the missing dipole dispersion suppressor..
 - 1st dipole creates dispersion wave,
 - 2nd dipole creates dispersion wave but with opposite sign
- design phase advance $\Delta\mu := \pi$

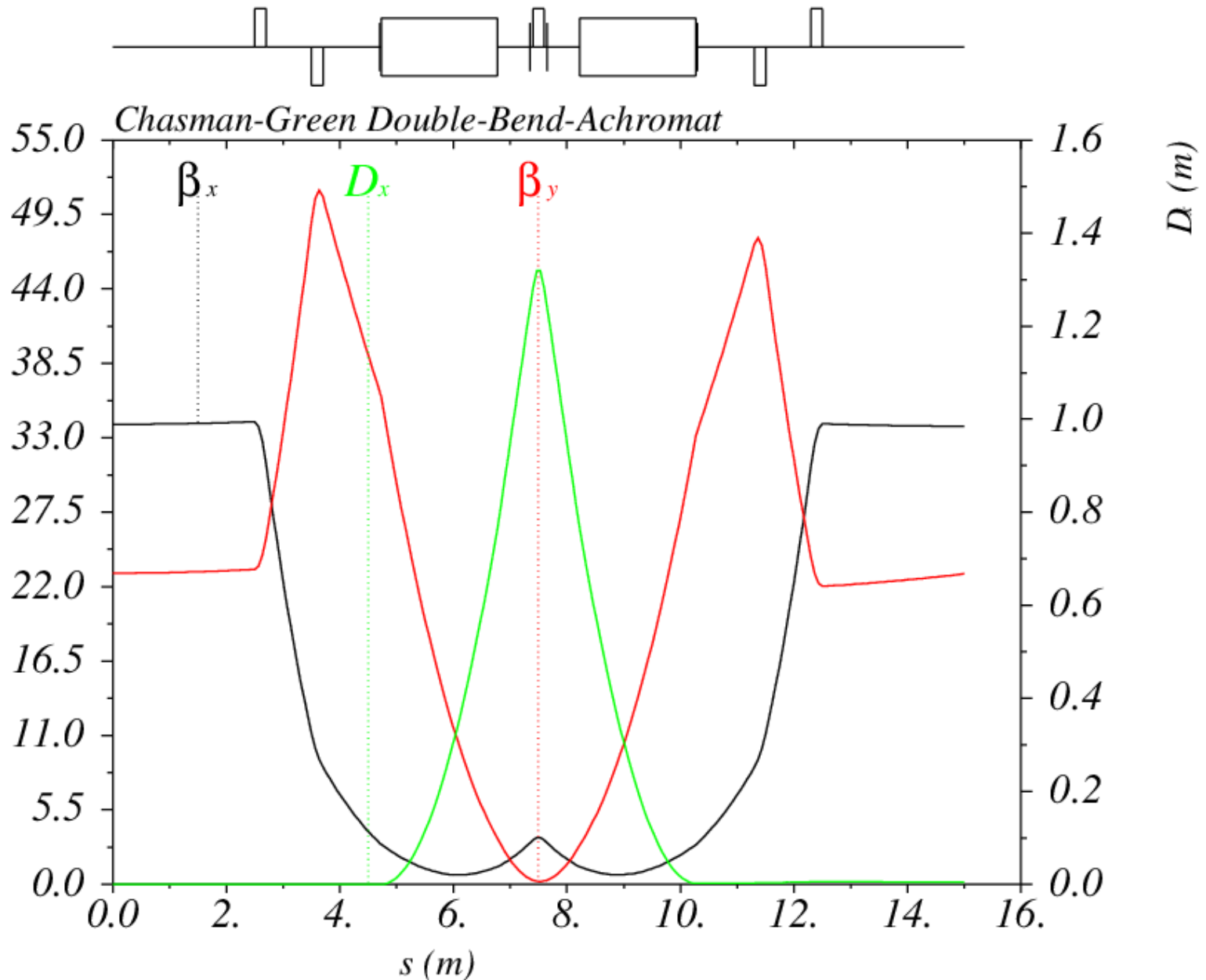


$$\frac{1}{b} + \frac{1}{g} = \frac{1}{f}$$

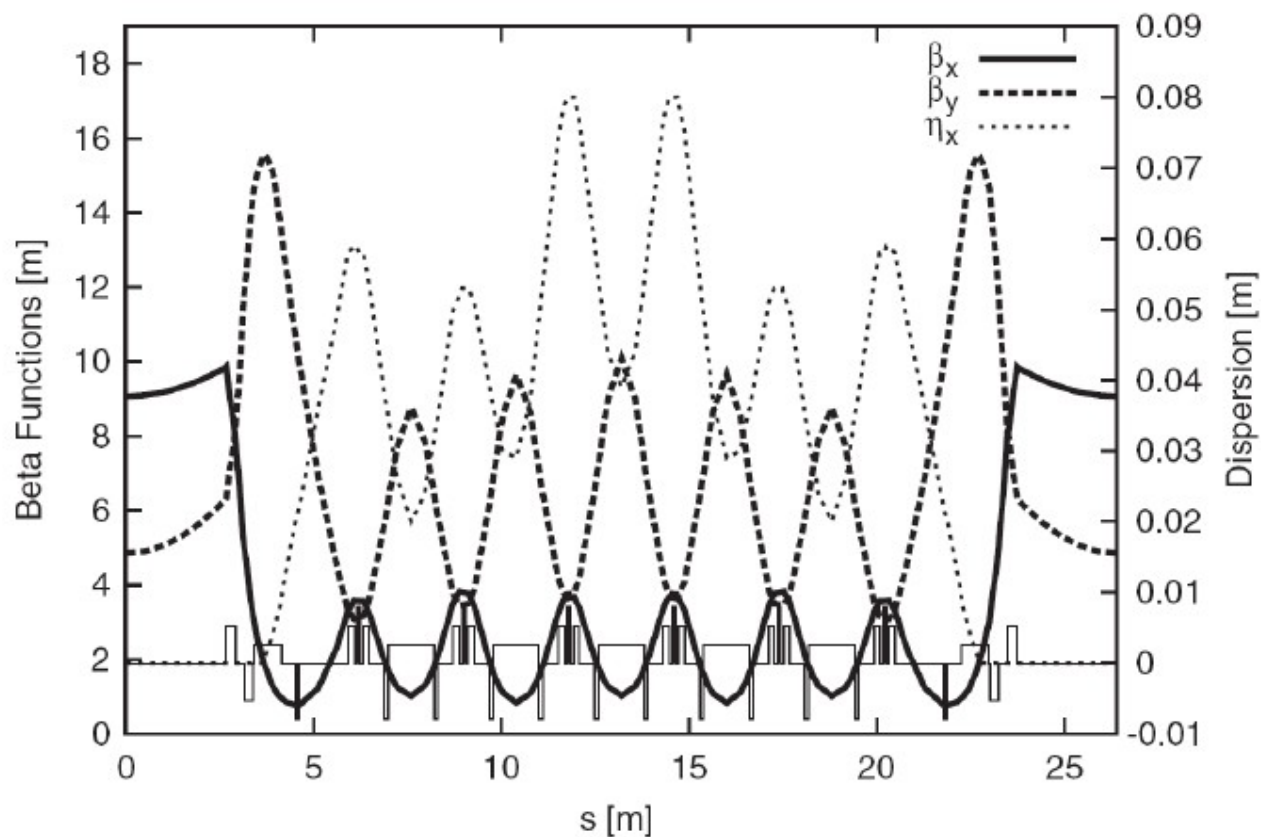
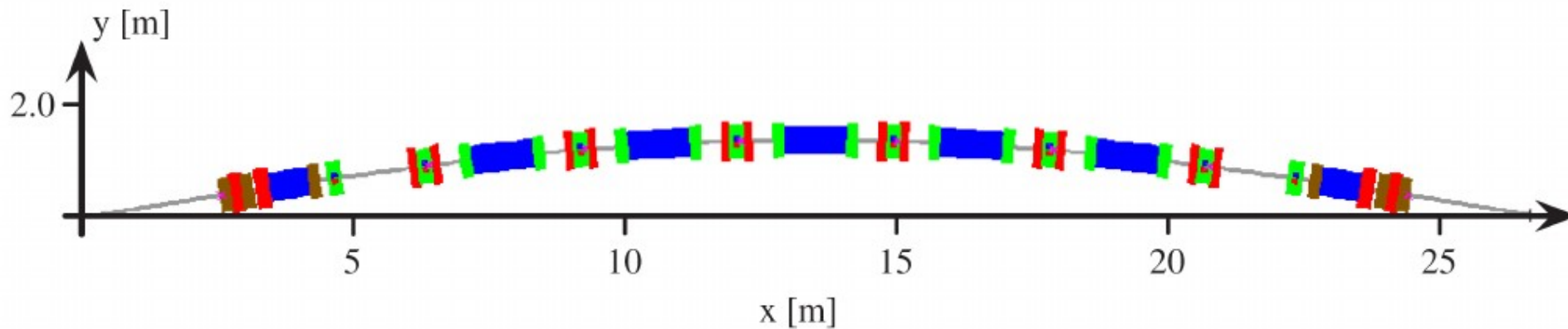
$$f = L/4$$

$$\frac{1}{f} = k \cdot L_{QF} = \frac{4}{L}$$

Chasman-Green Double-Bend Achromat II/II



Seven-Bend Achromat



S.C. Leeman et al, "Beam dynamics and expected performance of Sweden's new storage-ring light source: MAX IV," PRST-AB 12, 120701 (2009).

