

Introduction to RF – Part I

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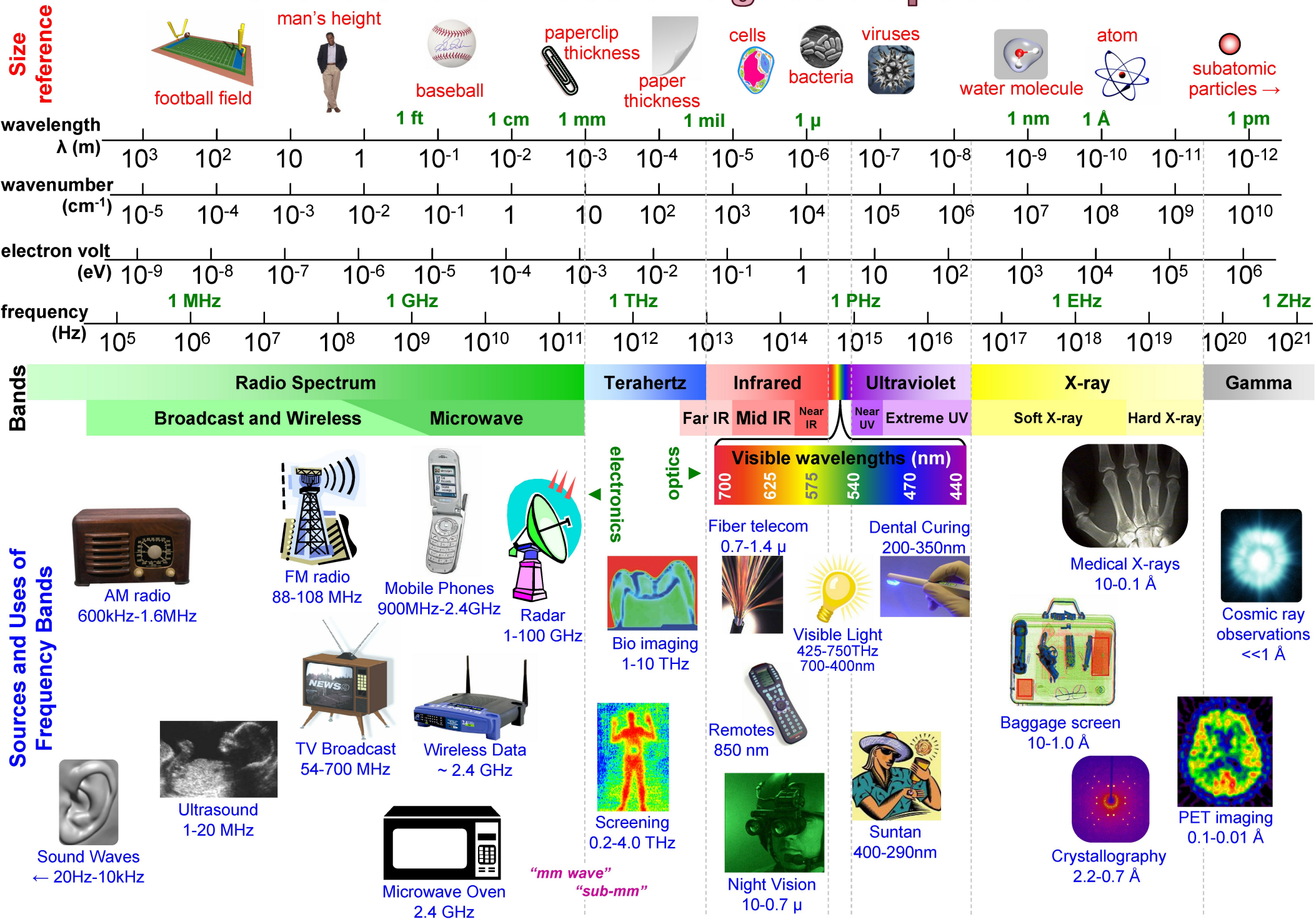


- Acknowledgements: F. Caspers, M. Betz, E. Jensen et al.
- Excellent online resource: <http://www.microwaves101.com/>

Introduction to RF – Part I

- Aim: Learn how high-frequency signals are measured
- Part I – time-domain vs. frequency domain (RF Detectors and Mixers)
 - Bode plots, power and dB(m, c, uV) definitions,
 - AM vs. FM vs. PM modulation
 - RF (Schottky) Diodes → RF Detectors (homodyne detection)
 - RF Mixers (heterodyne detection)
 - Introduction to: oscilloscopes, spectrum analyser, vector network analyser
- Laboratory:
 - some simple simulations using QUCS – guided/students
 - in || lab measurement with generator + spectrum analyser
 - some simple simulations using QUCS – guided/student
 - “Play” with BPM mock-up
 - Repeat in || previous day experience now with some active elements

Chart of the Electromagnetic Spectrum



$$\lambda = 3 \times 10^8 / \text{freq} = 1 / (\text{wn} * 100) = 1.24 \times 10^{-6} / \text{eV}$$

Decibel (dB)

- Convenient logarithmic measure of a power ratio.
- A “Bel” (= 10 dB) is defined as a power ratio of 10^1 .
- Consequently, 1 dB is a power ratio of $10^{0.1} \approx 1.259$
- If rdb denotes the measure in dB, we have:
 - N.B. 10 dB a factor 10 in power but factor 100 in amplitude!

$$r \text{ [dB]} = 10 \cdot \log\left(\frac{P}{P_0}\right) = 10 \cdot \log\left(\frac{A^2}{A_0^2}\right) = 20 \cdot \log\left(\frac{A}{A_0}\right)$$

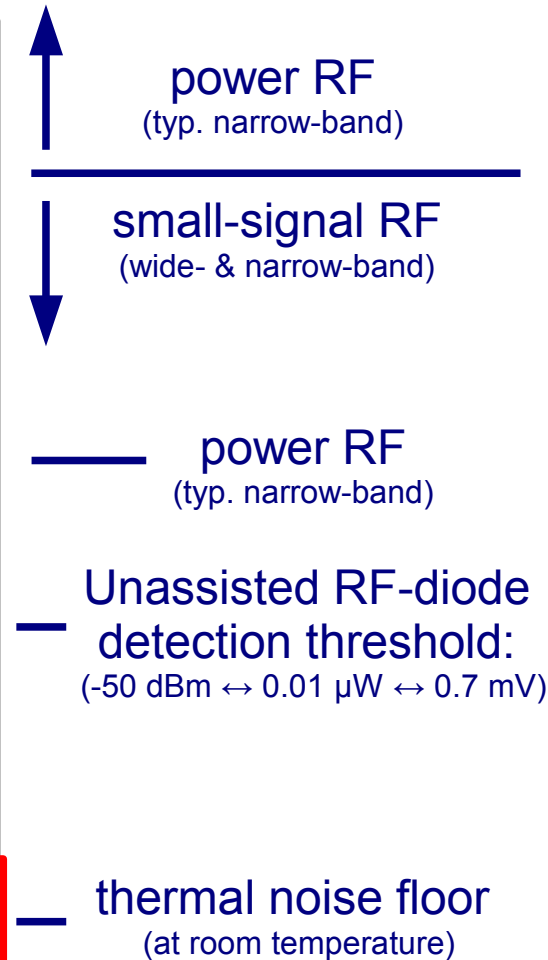
- Related: dBm ($P_0=1$ mW), dB μ V ($A_0=1$ μ V), dBc (P_0 being the carrier)

Decibel (dB) – Cont'd

- $10\text{mW} = 10\text{dBm}$, $0\text{dBm} = 1\text{mW}$
- $-110\text{ dBm} = 10^{-11}\text{mW} = 0.00001\text{nW}$
 - For a 50 ohm load : $-110\text{dBm} \leftrightarrow 0.7\ \mu\text{V}$, i.e. not much!
- Rule of thumb:
 - Double the power = 3 dB increase
 - Half the power = 3 dB decrease
- Common ranges (assuming 50 Ohm load)
 - 0-30 dBm small-signal RF amplifiers
 - typ. RF-diode detection threshold: $-50\text{ dBm} \leftrightarrow 0.01\ \mu\text{W} \leftrightarrow 0.7\ \text{mV}$

Common Power Levels

W	dBW $10 \cdot \log_{10}(P)$	dBm $10 \cdot \log_{10}(1000 \cdot P)$	V $\sqrt{50P}$ (w/ 50Ω)
1.000	0	+30	7.071
0.032	-15	+15	1.257
0.020	-16.990	+13.010	1.000
0.010	-20	+10	0.707
0.003	-25	+5	0.397
0.001	-30	0	0.224
316.2μW	-35	-5	0.126
100μW	-40	-10	0.071
0.1nW	-100	-70	70.71μV
0.1pW	-130	-100	2.236μV
10fW	-140	-110	0.707μV
1fW	-150	-120	0.224μV
4.142E-21 (kT at 300K)	-203.8	-173.8	0.455nV



Fourier Transform I

- An arbitrary signal $g(t)$ can be expressed frequency-domain using the Fourier transform (FT):

$$\begin{aligned}\mathcal{F}\{g(t)\} &= G(\omega) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{+\infty} g(t) e^{+j\omega t} dt \\ \mathcal{F}^{-1}\{G(\omega)\} &= G(t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{+\infty} G(\omega) e^{-j\omega t} d\omega\end{aligned}$$

- Many problems dealing with linear-time-invariant (LTI) systems are much easier described in frequency domain
- FT Cousins:
 - Laplace Transform: $j\omega \rightarrow s$, and integrating only from '0' rather than $-\infty$
 - Strictly causal \rightarrow used in system- and control theory
 - Z-Transform:
 - $\rightarrow z = e^{j\omega T}$, with T being the sampling period
 - delays of $k \cdot T$ become z^k

Fourier Transform II

Linearity: $\mathcal{F}(af(t)) = a\mathcal{F}(f(t))$

Superposition: $\mathcal{F}(af(t)+bg(t)) = aF(\omega)+bG(\omega)$

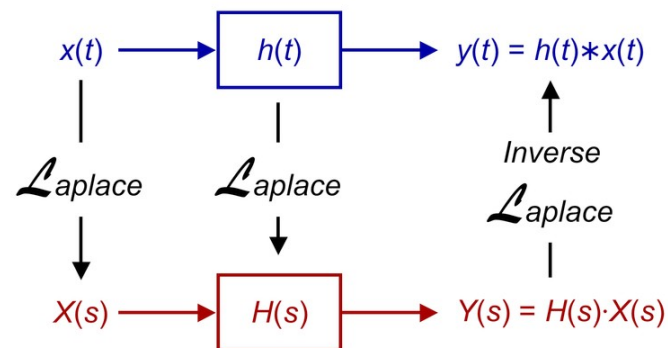
Time Delay: $\mathcal{F}(f(t-\Delta t)) = e^{-j\omega\Delta t}F(\omega)$

Frequency Shift: $\mathcal{F}(f(t)\cdot e^{-j\omega_0 t}) = F(\omega-\omega_0)$

Time Scaling: $\mathcal{F}(f(at)) = \frac{1}{|a|}F\left(\frac{\omega}{a}\right)$

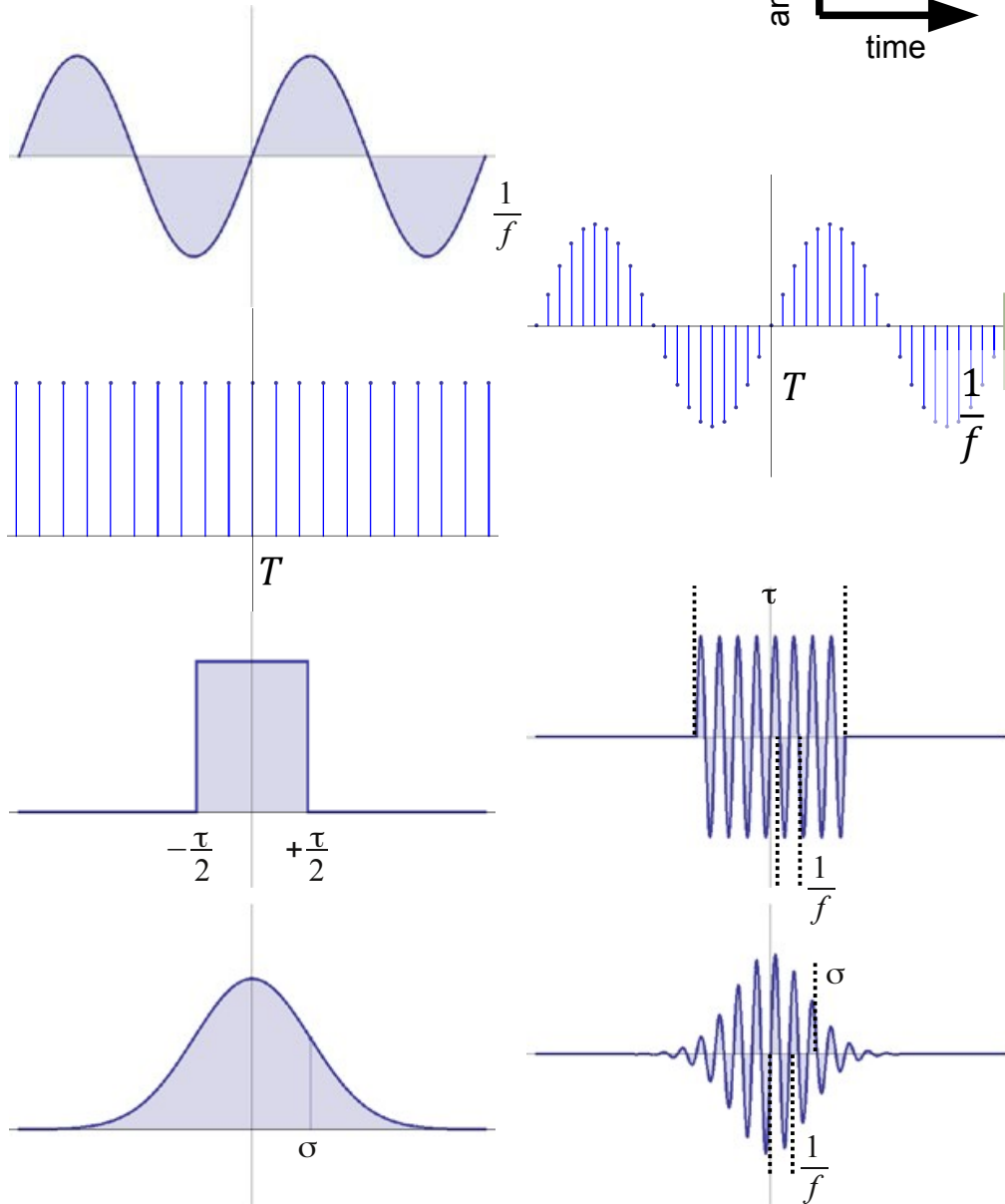
Differentiation: $\mathcal{F}\left(d^k f \frac{(t)}{dt^k}\right) = (j\omega)^k F\left(\frac{\omega}{a}\right)$

Convolution: $\mathcal{F}(f(t)\cdot g(t)) = F(\omega)*G(\omega)$, and
 $\mathcal{F}(f(t)*g(t)) = F(\omega)\cdot G(\omega)$

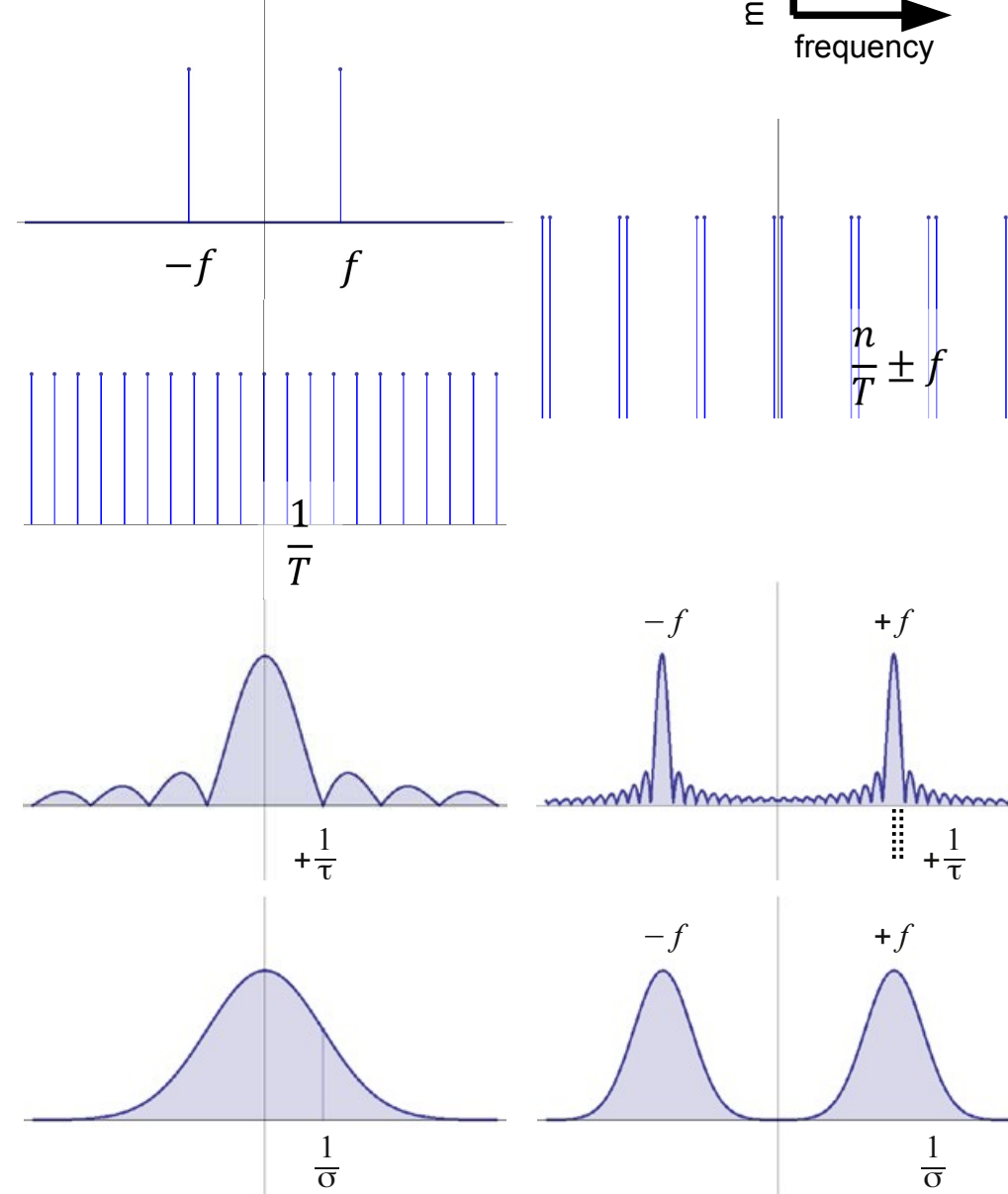


Fourier Transform III – Examples

Time-Domain

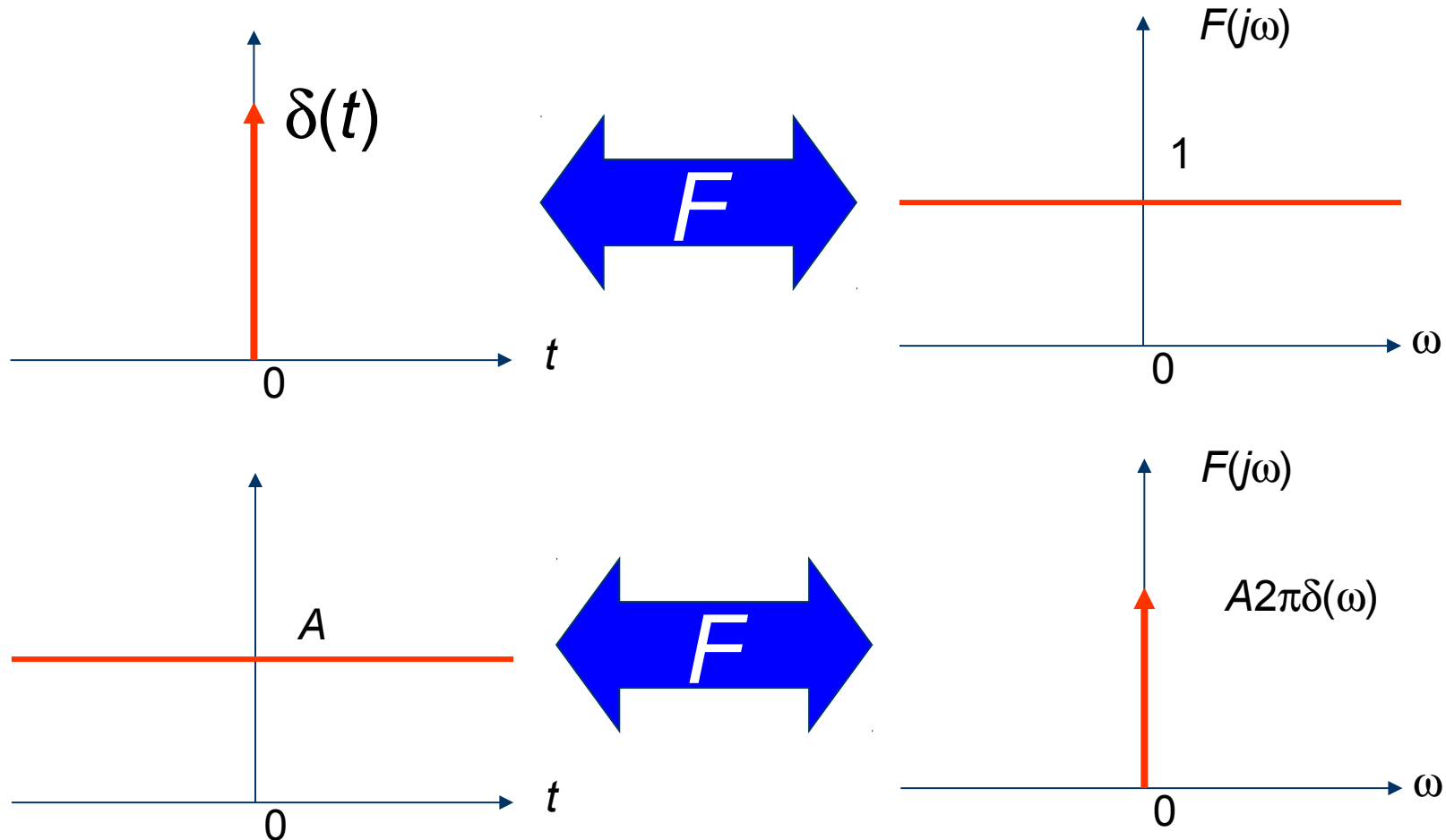


Frequency Domain



Some important special Functions I/II

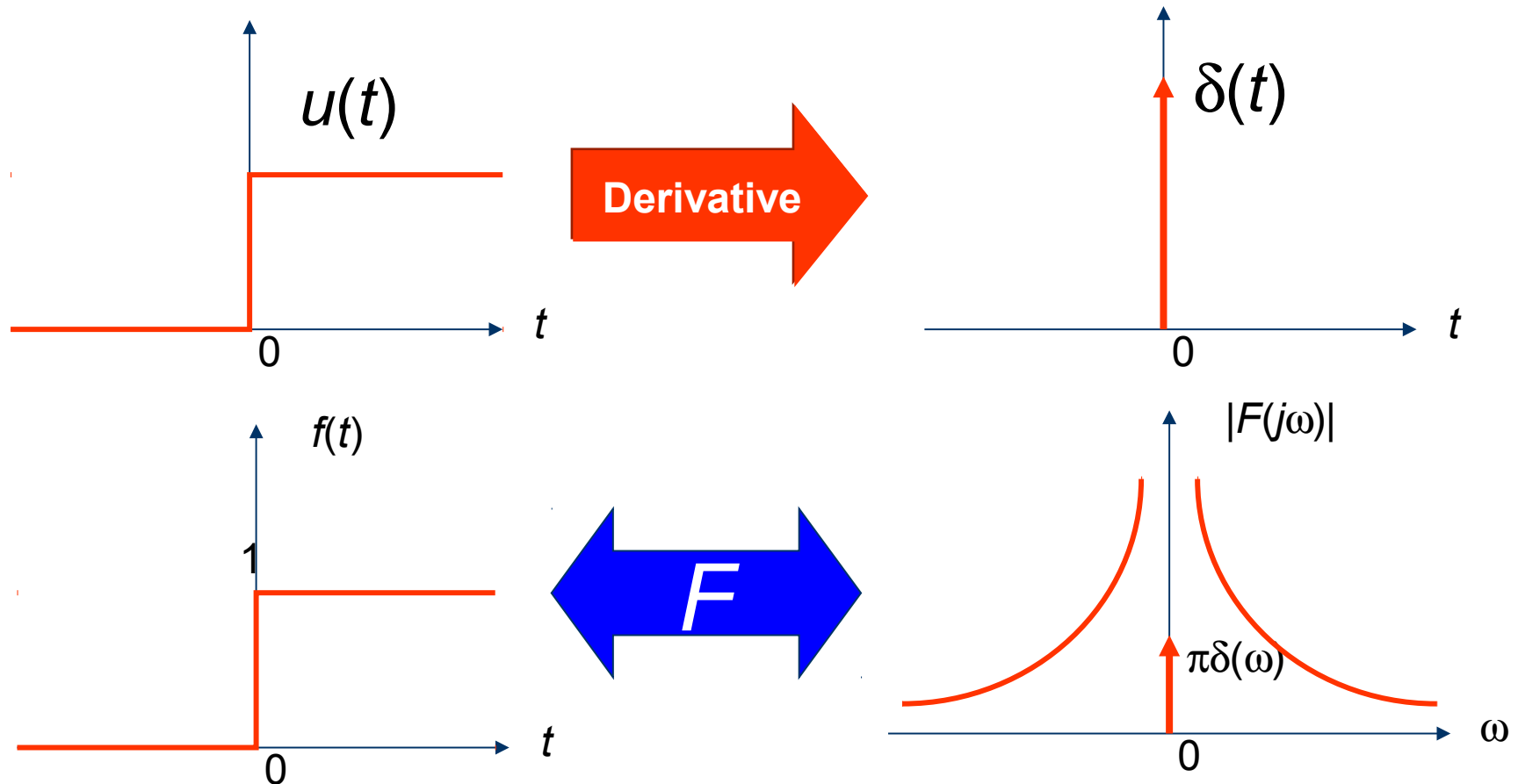
- Dirac delta function (theory) or 'impulse function' (praxis):



- Often used to decompose and analyse arbitrary wide-band signal, i.e. to measure system response

Some important special Functions II/II

- Heaviside step function:



- Equivalent to dirac delta-based analysis but in praxis more easy to use and produce experimentally

Fixed Frequency Oscillation & Phasor

- Steady-state frequency solution can be decomposed:

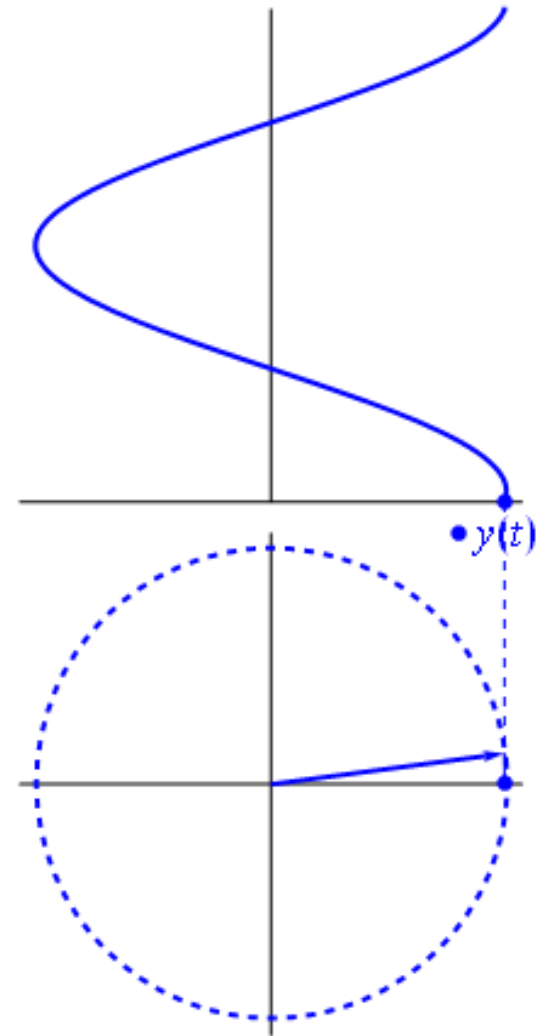
$$A \cos(\omega t - \varphi) = A \cos(\omega t)\cos(\varphi) + A \sin(\omega t)\sin(\varphi)$$

- can be interpreted as the projection on the real axis of a circular motion in the complex plane.

$$\Re \left\{ A \left[\cos(\varphi) + j \sin(\varphi) \right] \cdot e^{j\omega t} \right\}$$

- The complex amplitude is called “phasor”;

$$\tilde{A} = A \left[\cos(\varphi) + j \sin(\varphi) \right]$$

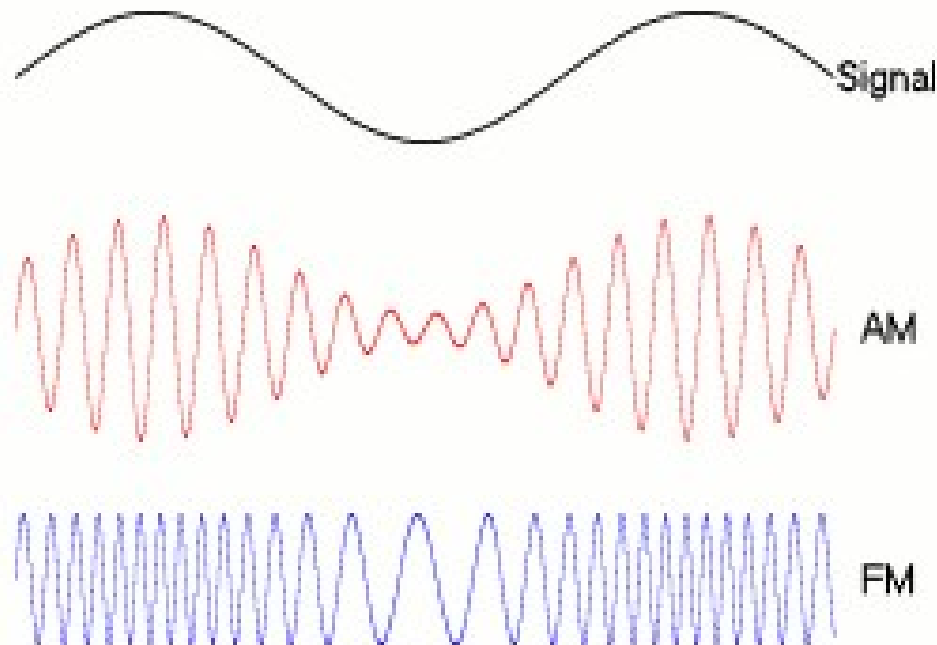


Amplitude, Frequency & Phase Modulation I/III

$$f_{AM}(t) = A_0 \cdot (1 + m \cos(\omega_s t)) \cdot \cos(\omega_c t)$$

$$f_{FM}(t) = A_0 \cdot \cos\left(\omega_c t + \underbrace{\frac{\Delta \omega}{\omega_m}}_{:=m} \cos(\omega_m t)\right)$$

- modulation index m : maximum relative amplitude resp. frequency deviation



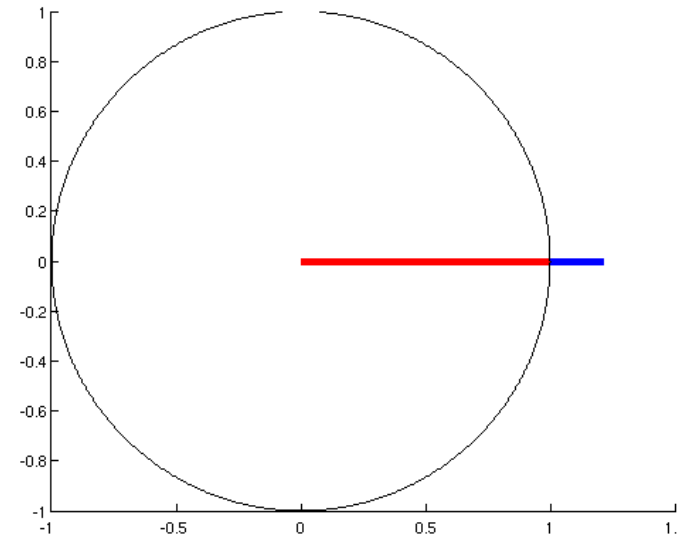
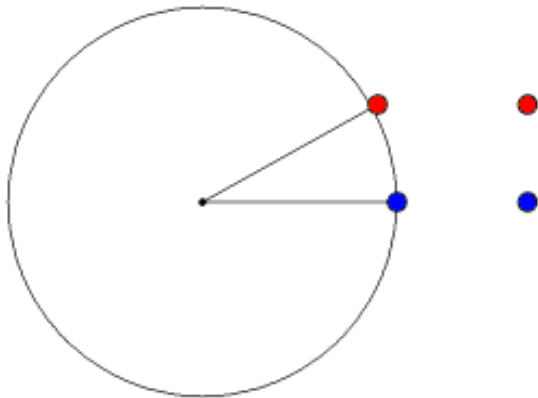
Amplitude, Frequency & Phase Modulation I/III

$$f_{AM}(t) = A_0 \cdot \Re \left\{ \left(1 + \frac{m}{2} e^{+j\omega_m t} + \frac{m}{2} e^{-j\omega_m t} \right) e^{j\omega_c t} \right\}$$

$$f_{FM}(t) = A_0 \cdot \Re \left\{ e^{+j\omega_m t + m \sin(\omega_m t)} \right\} = A_0 \cdot \Re \left\{ \sum_{n=-\infty}^{n=+\infty} J_n(m) e^{+j(\omega_c t + n \cdot \omega_m)} \right\}$$

- modulation index m : maximum relative amplitude resp. frequency deviation

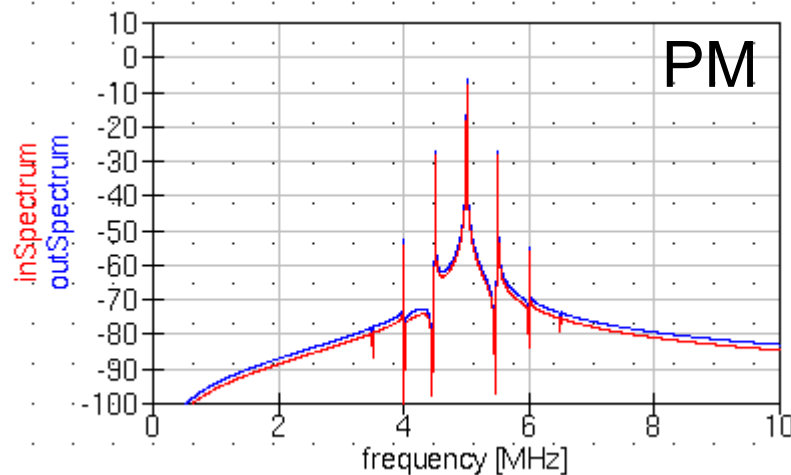
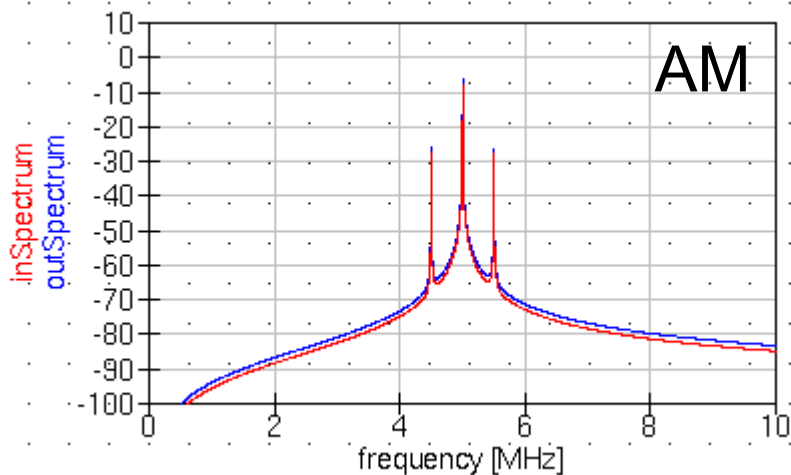
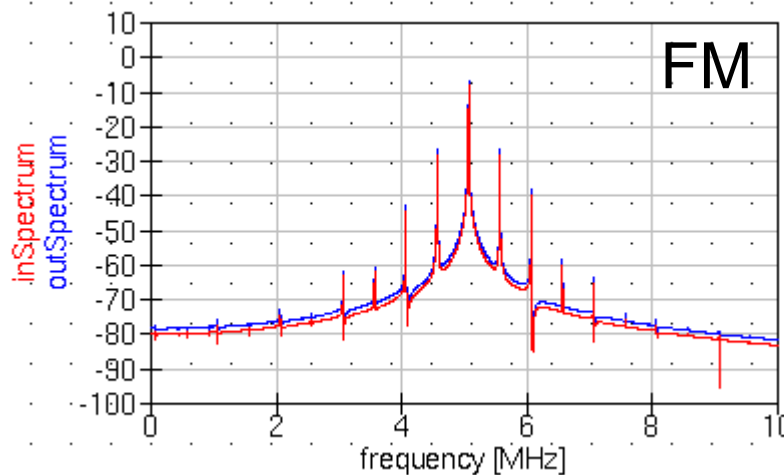
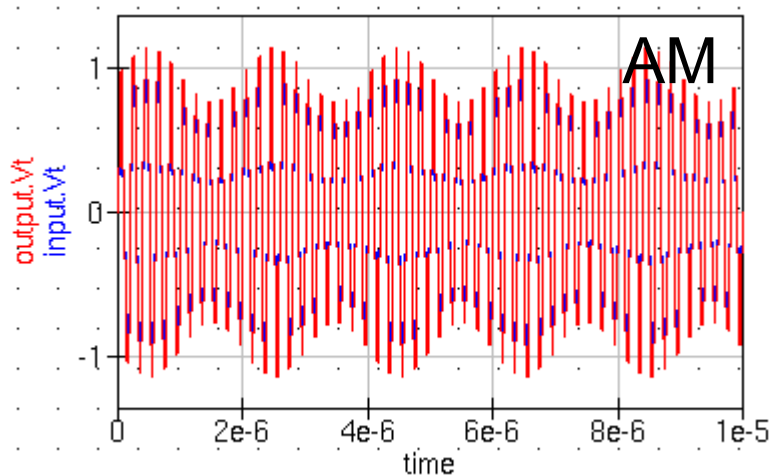
Image courtesy of whiteboard.ping.se



Amplitude, Frequency & Phase Modulation II/III

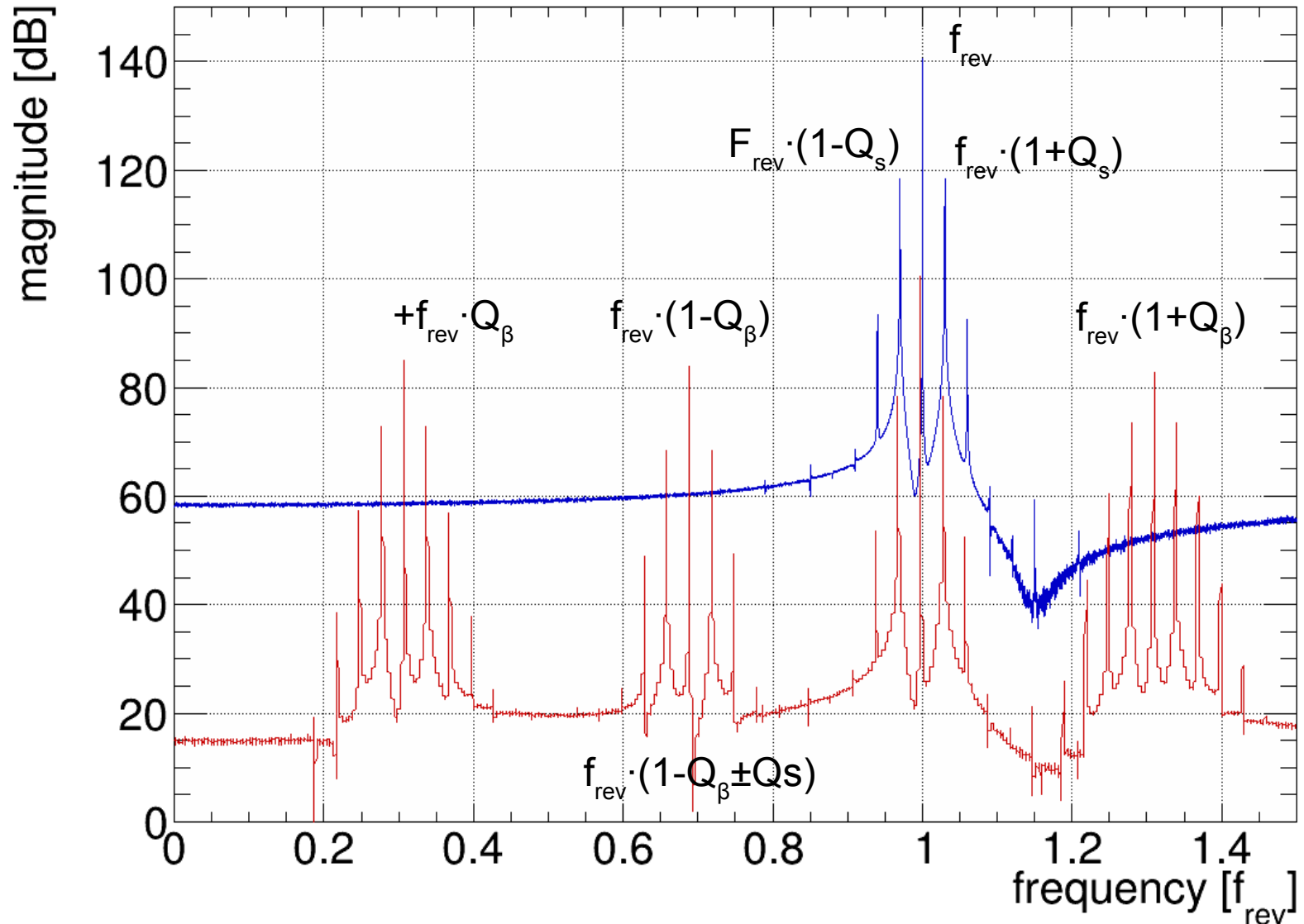
- Accelerator related examples

- AM: turn-by-turn transverse beam position or betatron (Q) motion
- FM: turn-by-turn longitudinal synchrotron motion (arrival time at pick-up)



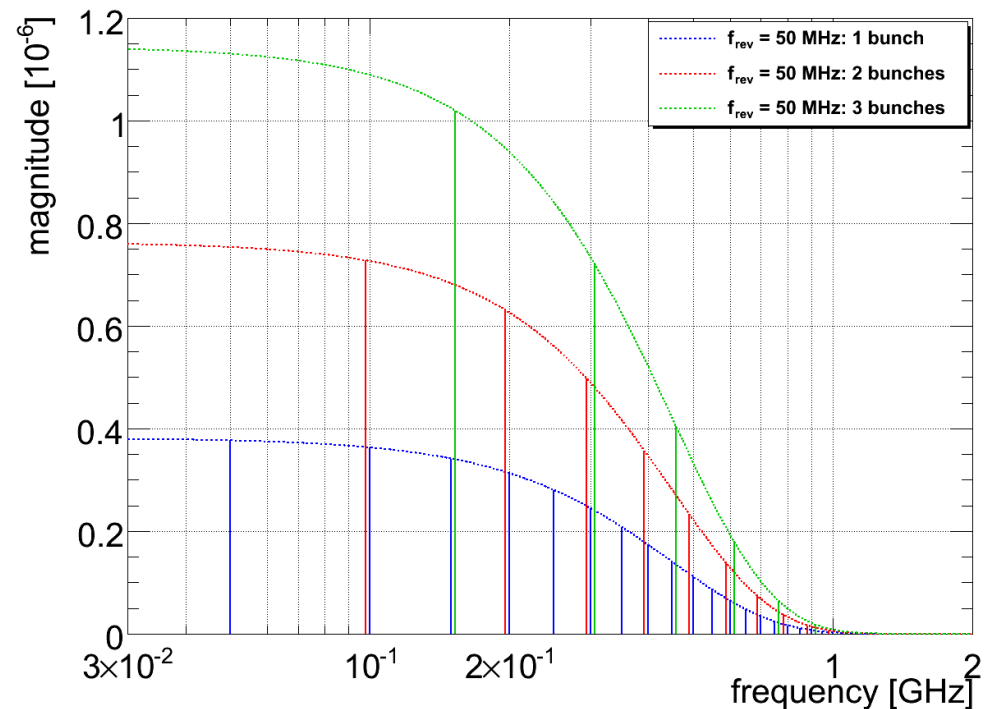
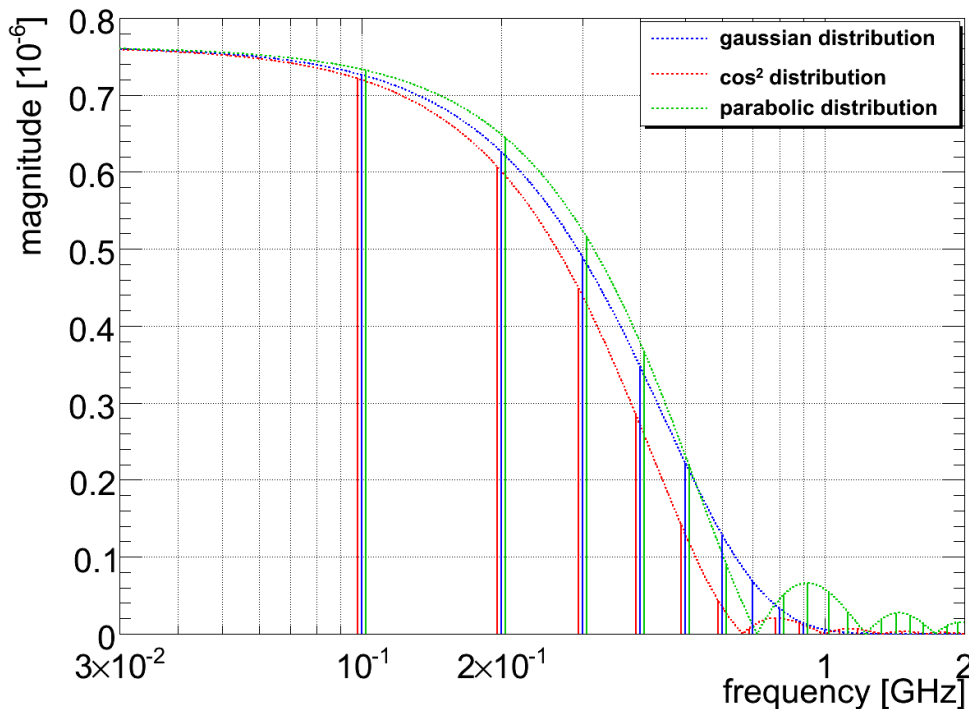
Amplitude, Frequency & Phase Modulation III/III

- A more complex bunch spectrum...



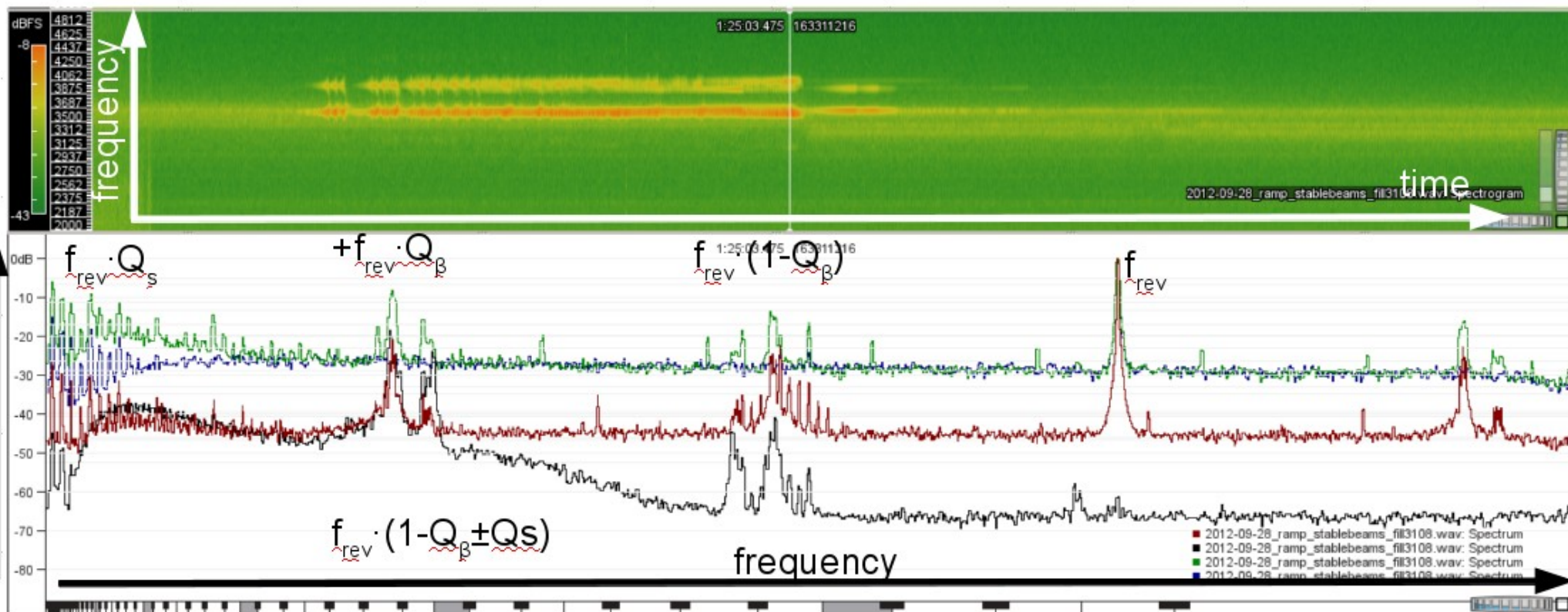
Beam Spectrum

- Typical beam structure isn't a perfect sine but short bursts of particles contained inside the RF separatrix (aka. RF bucket)
 - Periodic dirac delta $\mathcal{F}\{\sum_n \delta(n_{\text{turn}} \cdot (t - \Delta t_{\text{turn}}))\} \rightarrow \sum_n \delta_{\omega}(n/\Delta t_{\text{turn}})$
 - beam spectrum: $\mathcal{F}\{\rho_{\text{longitudinal}}(t) \cdot x_{\text{transverse}}(t)\} \rightarrow \rho_{\text{longitudinal}}(\omega) * X_{\text{transverse}}(\omega)$

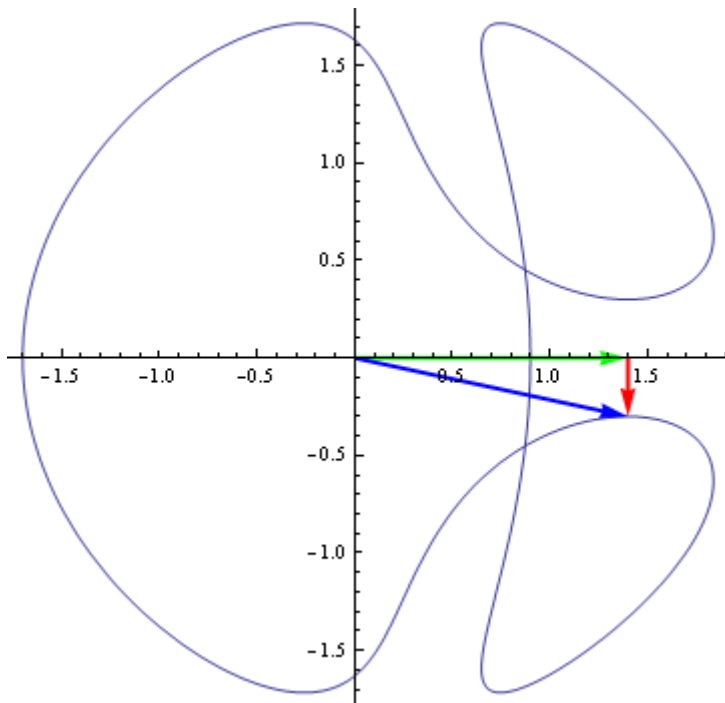
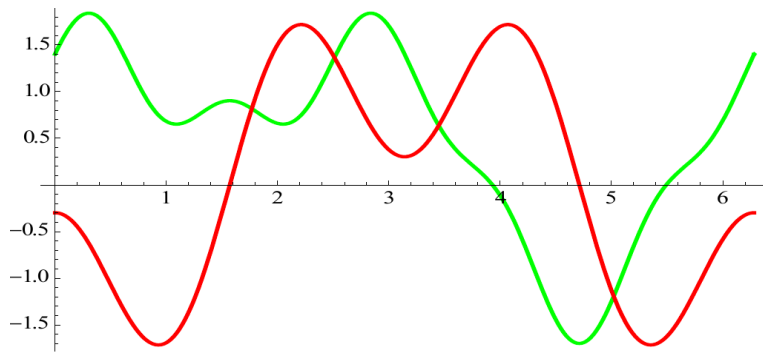


Transverse Tune Spectrum

- Still too easy?



IQ-Modulation



- More generally, a modulation can have both amplitude and phase modulating components. They can be described as the in-phase (I) and quadrature (Q) components in a chosen reference, $\cos(\omega_r t)$.

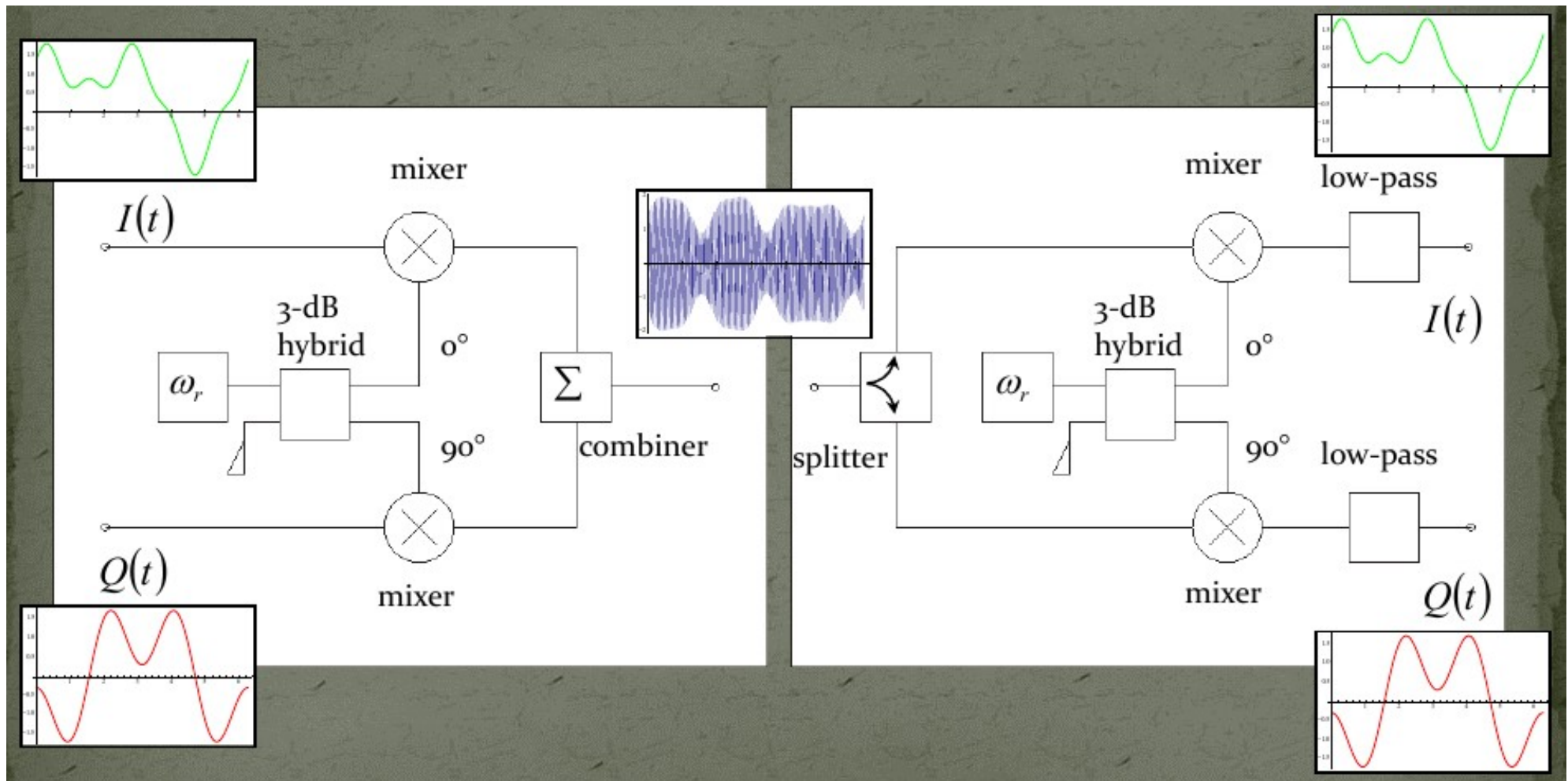
- In complex notation, the modulated cos RF is:

$$\begin{aligned} \operatorname{Re} \left\{ (I(t) + j Q(t)) e^{j \omega_r t} \right\} &= \\ \operatorname{Re} \left\{ (I(t) + j Q(t)) (\cos(\omega_r t) + j \sin(\omega_r t)) \right\} &= \\ I(t) \cos(\omega_r t) - Q(t) \sin(\omega_r t) & \end{aligned}$$

- I and Q are the Cartesian coordinates in the complex “Phasor” plane, where amplitude and phase are the corresponding polar coordinates.
 - $I(t) = A(t) \cos(\varphi)$
 - $Q(t) = A(t) \sin(\varphi)$

IQ-Modulator and Demodulator

- Combination of AM- and FM- modulation
 - Basically the analog equivalent of the sin-cos Fourier transform definition

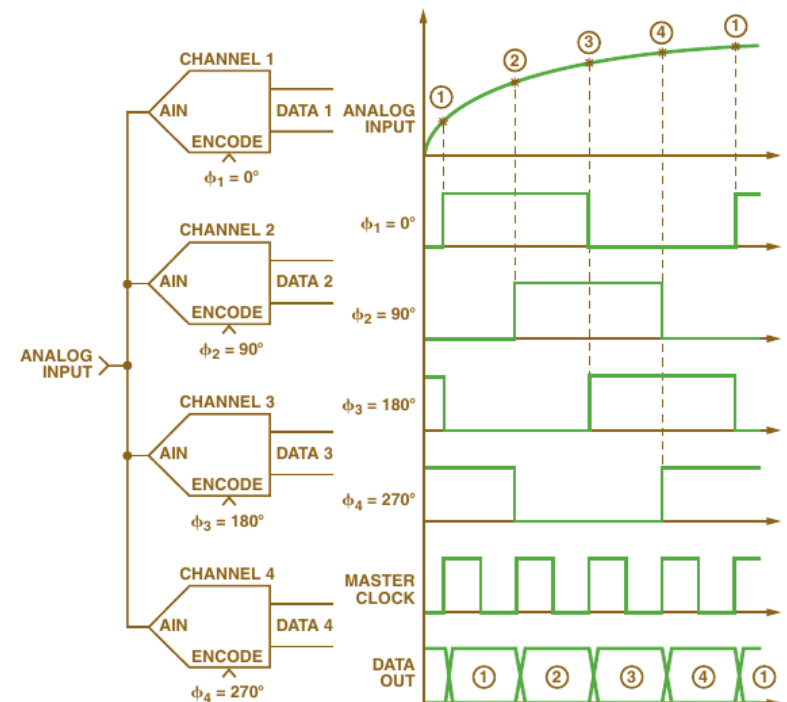


Direct Time-Domain Observation

- Oscilloscope (or. 'scope'):
direct sampling in **time domain**

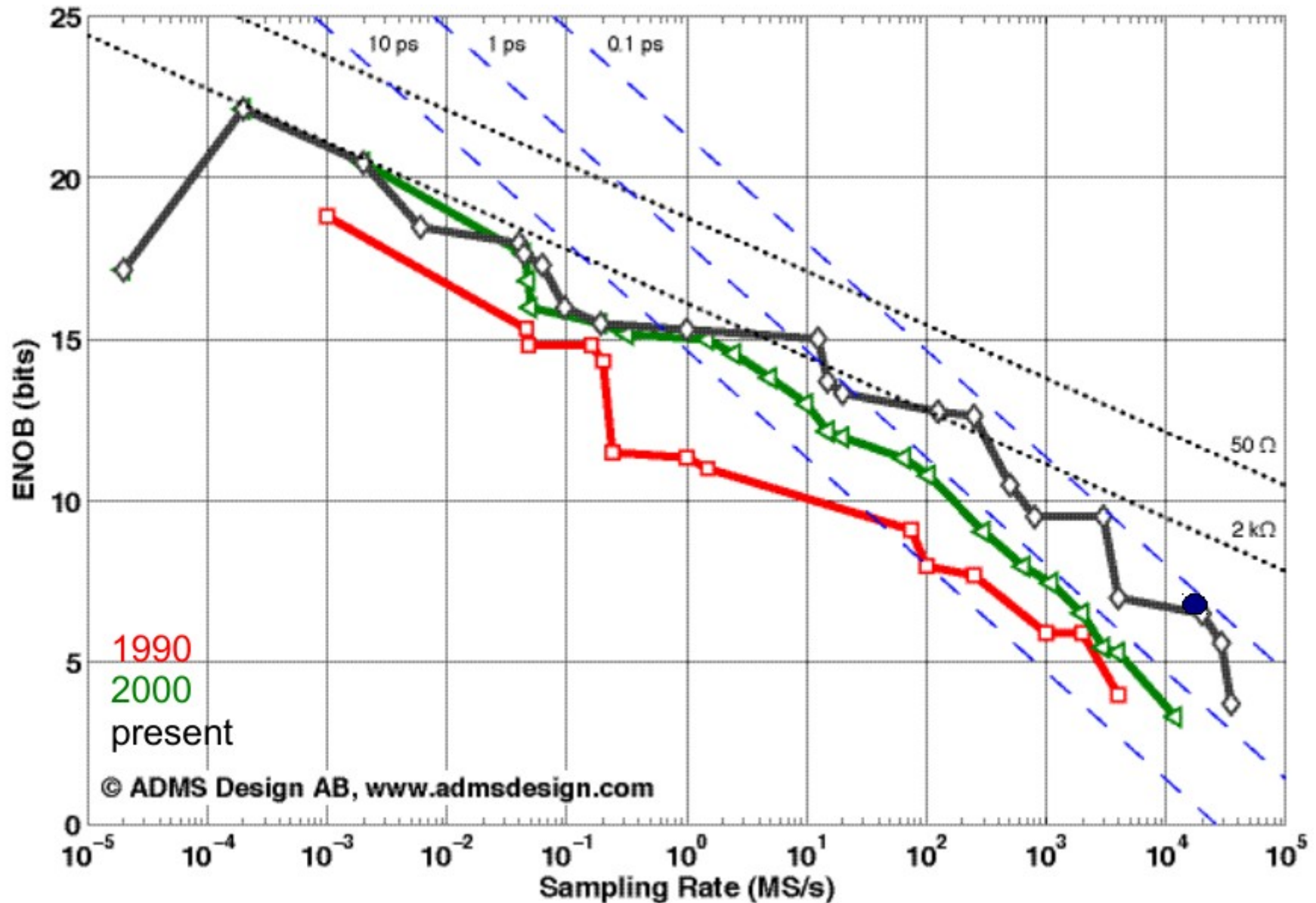


- periodic signals, burst signal
- typ. application: e.g. direct observation of pick-up signal
- post-processing: e.g. fourier transform → wide-band spectrum analyser
- sampling speeds and bandwidths: 500 MHz → >50 GHz
 - N.B. price range: few k\$ → >200 k\$
- Limited maximum instantaneous voltage range $U_{\max}/U_{\min} \approx 100$



Limits of direct time-domain digitization

- ADCs performance levels out and approaching fundamental physical limits



The RF Detector Diode I

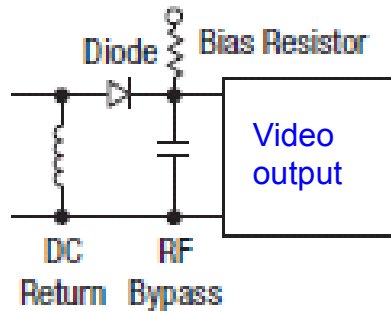
- We are not discussing the generation of RF signals here, just the detection
- Basic tool: fast RF diode (= Schottky diode)
 - In general, Schottky diodes are fast but still have a voltage dependent junction capacity (metal – semi-conductor junction)



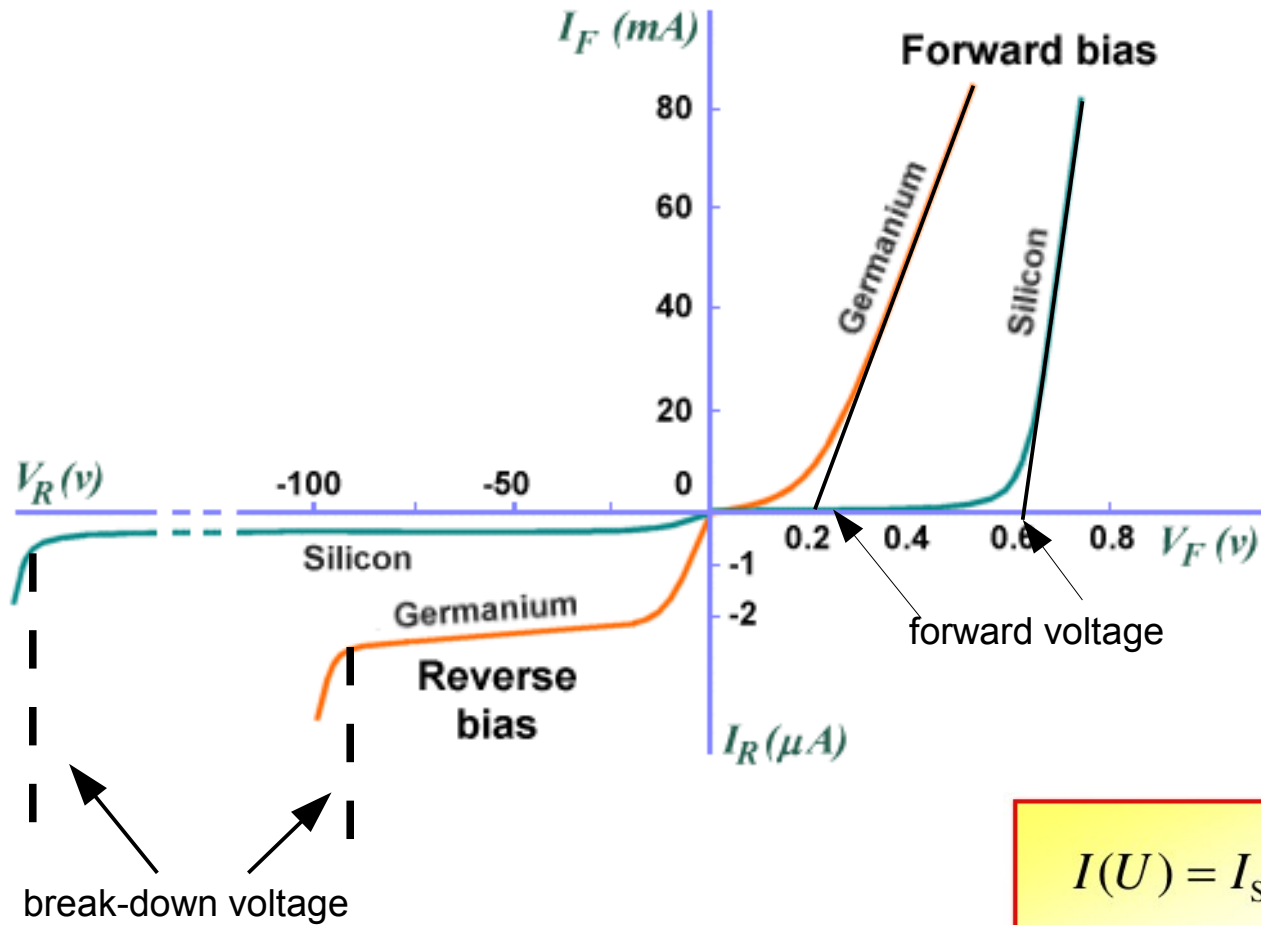
A typical RF detector diode

Try to guess from the type of the connector which side is the RF input and which is the output

- Equivalent circuit:



The RF Detector Diode II



$$I(U) = I_s \left(\exp\left(\frac{eU}{mkT}\right) - 1 \right)$$

$$= I_s \left(\exp\left(\frac{U}{mU_T}\right) - 1 \right)$$

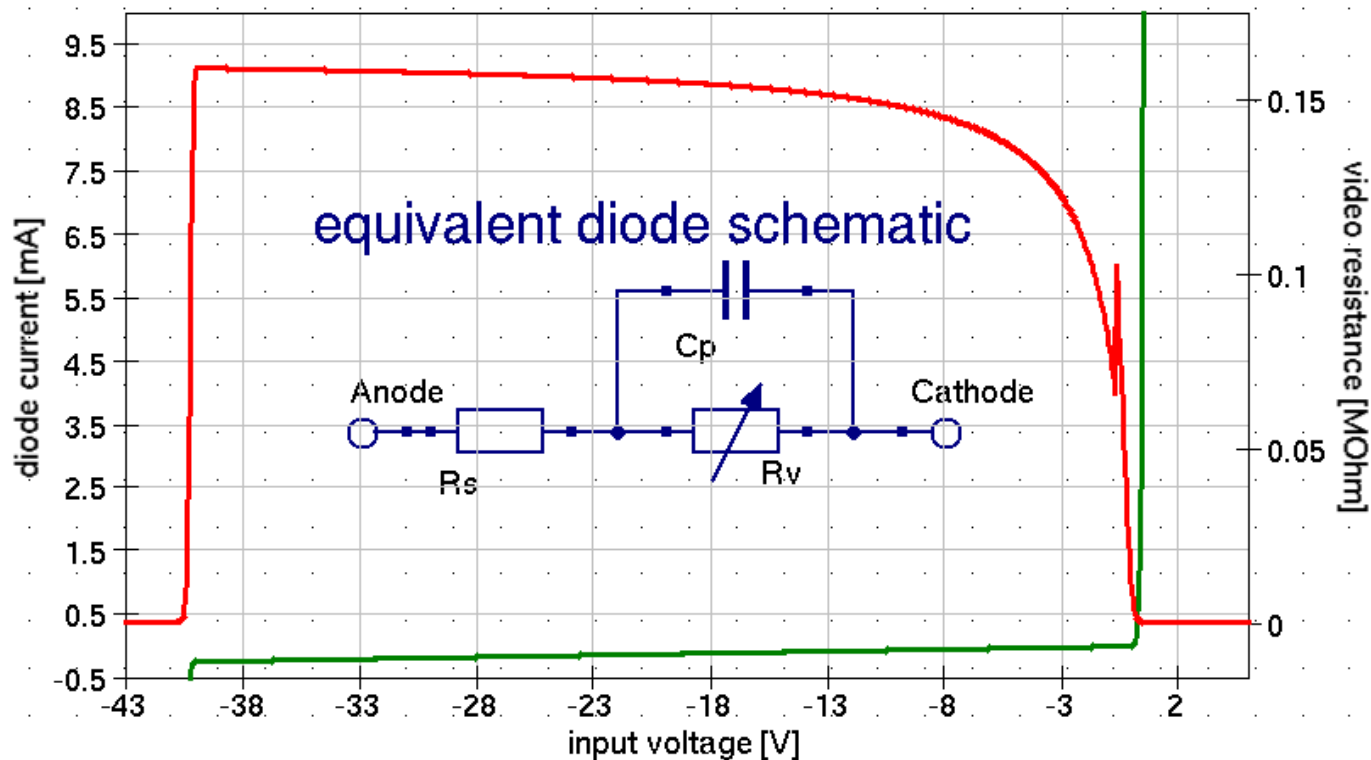
$$U_T = \frac{kT}{e} = 25.5 \text{ mV}$$

- Material properties
 - Silicon: $I_s = 10^{-11} \text{ A}$, $mU_T = 0.03 \text{ V}$
 - Germanium: $I_s = 10^{-7} \text{ A}$, $mU_T = 0.03 \text{ V}$

The RF Detector Diode III

- Equivalent diode circuit

- R_s : series resistance (Schottky: $R_s < \text{few } \Omega$)
- C_p : junction/parasitic capacitance (Schottky: $C_p < 1 \text{ pF} \leftrightarrow$ limits bandwidth)
- R_v : video resistance \rightarrow similar to a voltage controlled variable resistor
 - Very small resistance for positive voltage
 - Very large resistance for negative voltages



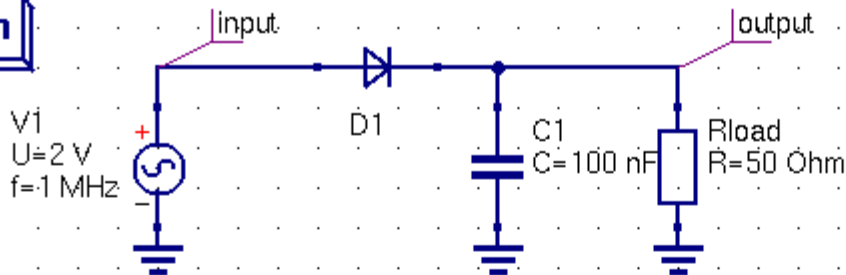
The RF Detector Diode IV – Rectifier

dc simulation

DC1

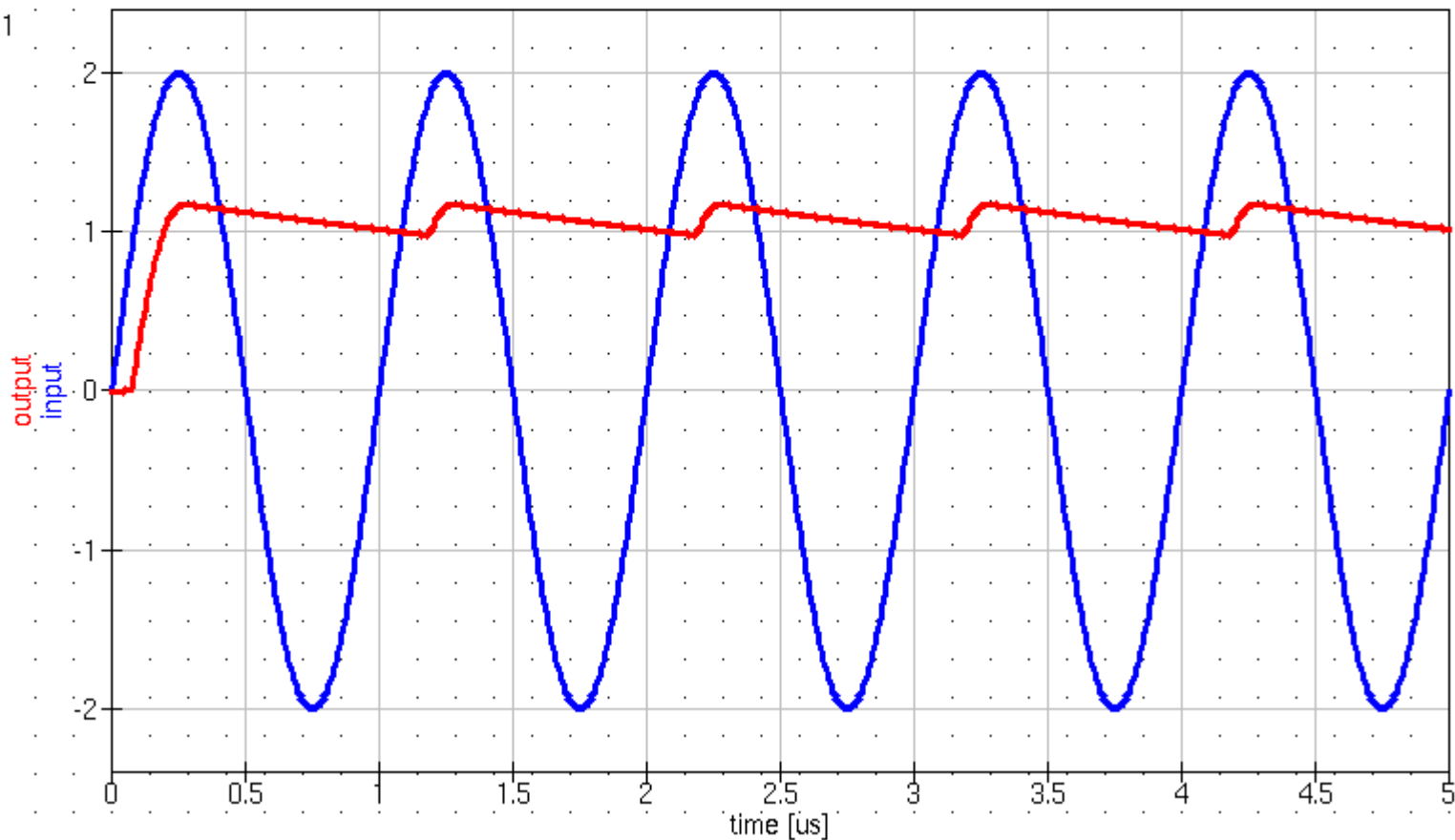
transient simulation

TR1
Type=lin
Start=0
Stop=5 us
Points=1001



Equation

Eqn1
time_us=time*1e6
input=PlotVs(input,Vt,time_us)
output=PlotVs(output,Vt,time_us)



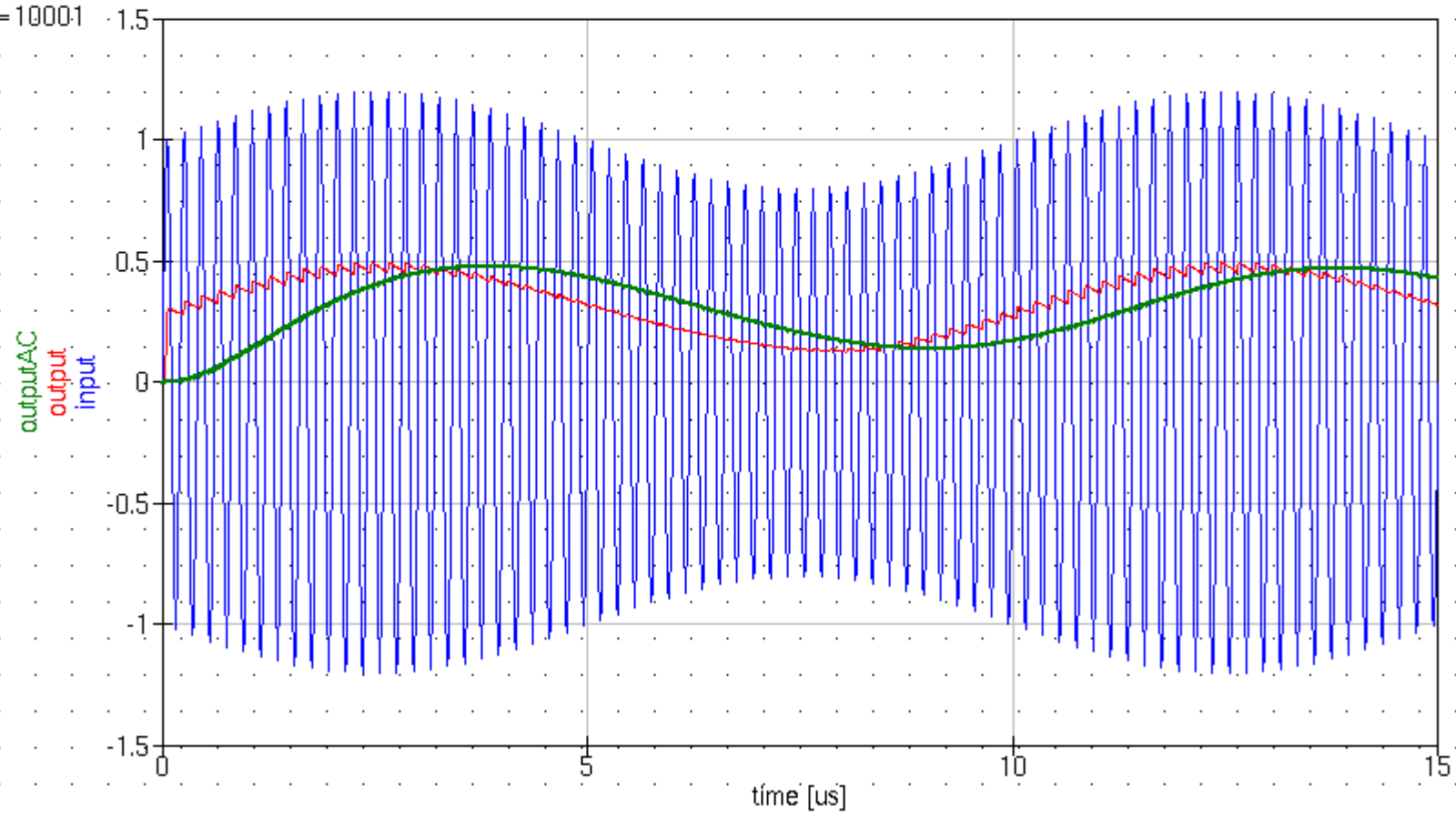
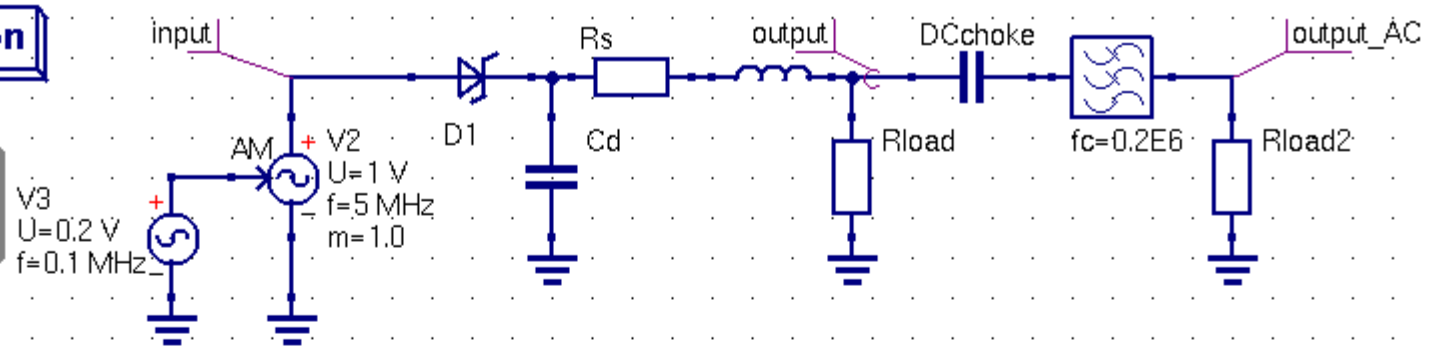
Simple RF Detector – Time Domain

dc simulation

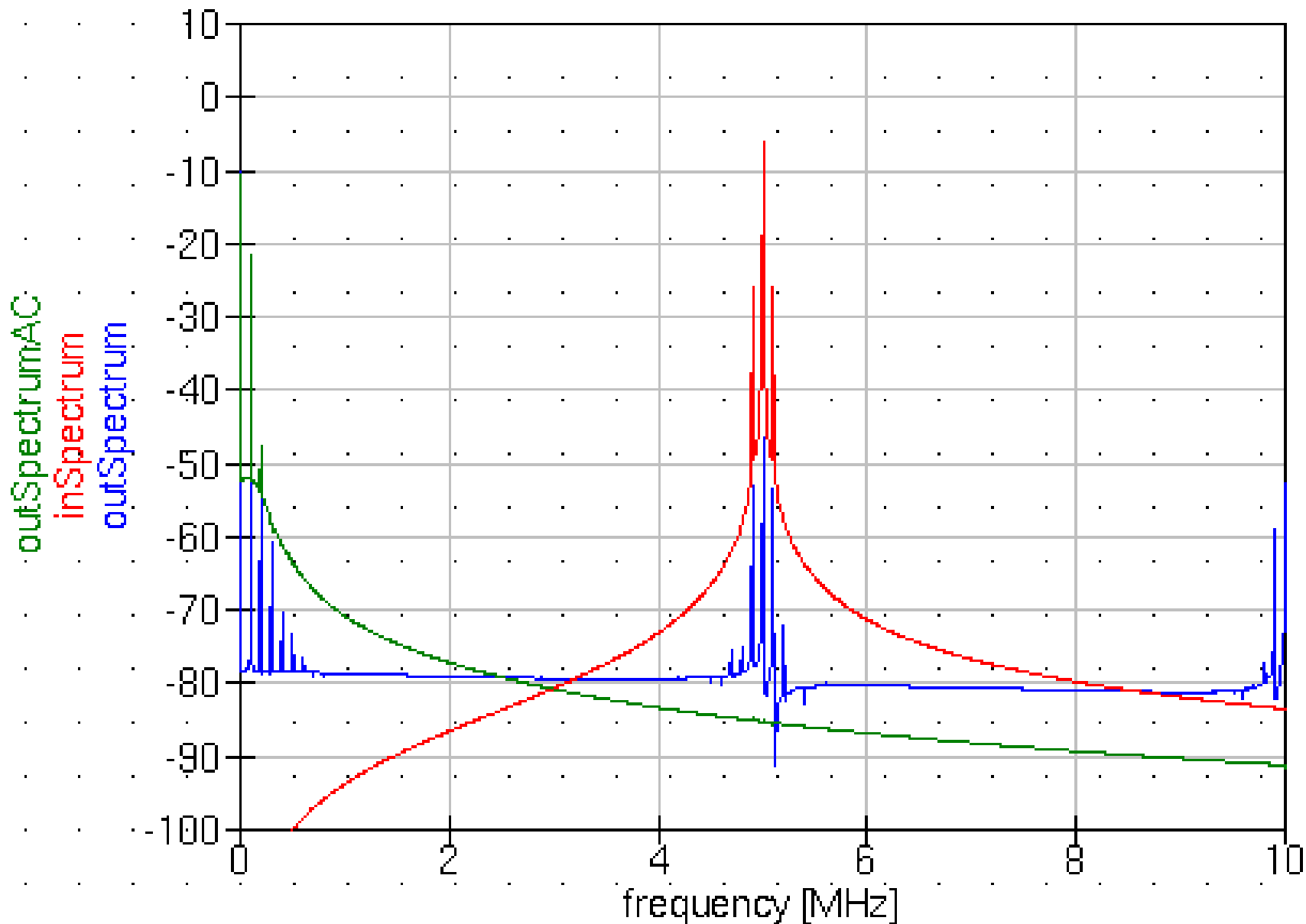
DC1

transient simulation

TR1
Type=lin
Start=0
Stop=100 us
Points=10001



Simple RF Detector – Frequency Domain



- This detection scheme is also referred to as 'homodyne detection'

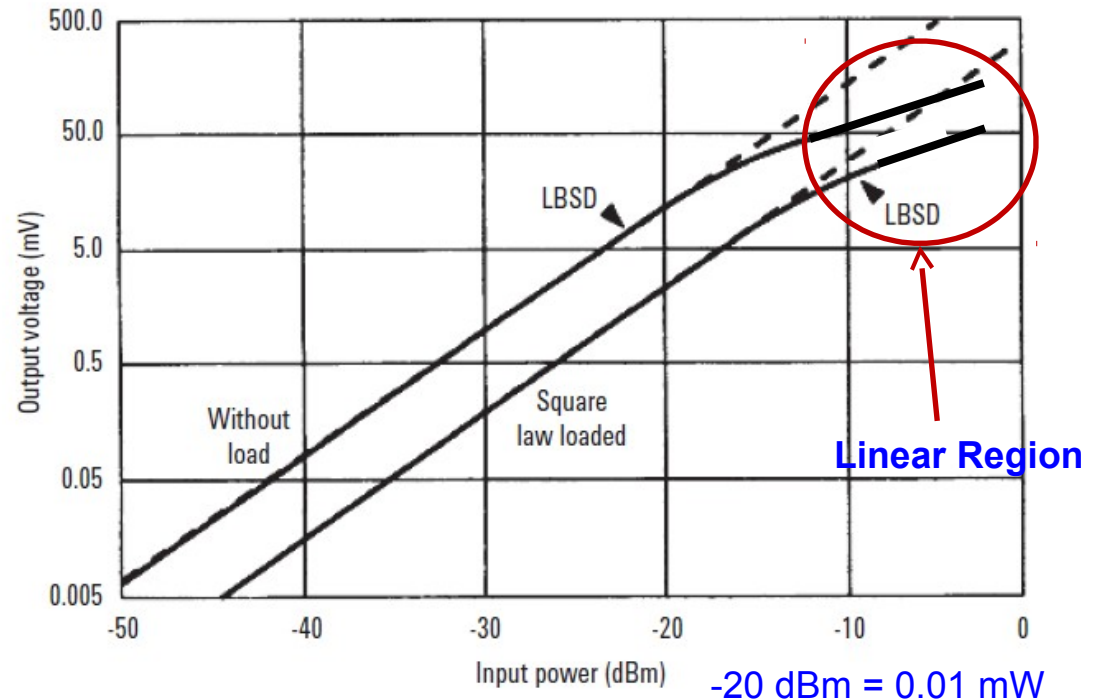
RF Diode – Square-Law

- This diagram depicts the so called square-law region where the output voltage (V_{Video}) is proportional to the input power

Since the input power is proportional to the square of the input voltage ($V_{\text{RF}2}$) and the output signal is proportional to the input power, this region is called square-law region.

$$V_{\text{Video}} \sim (V_{\text{RF}})^2$$

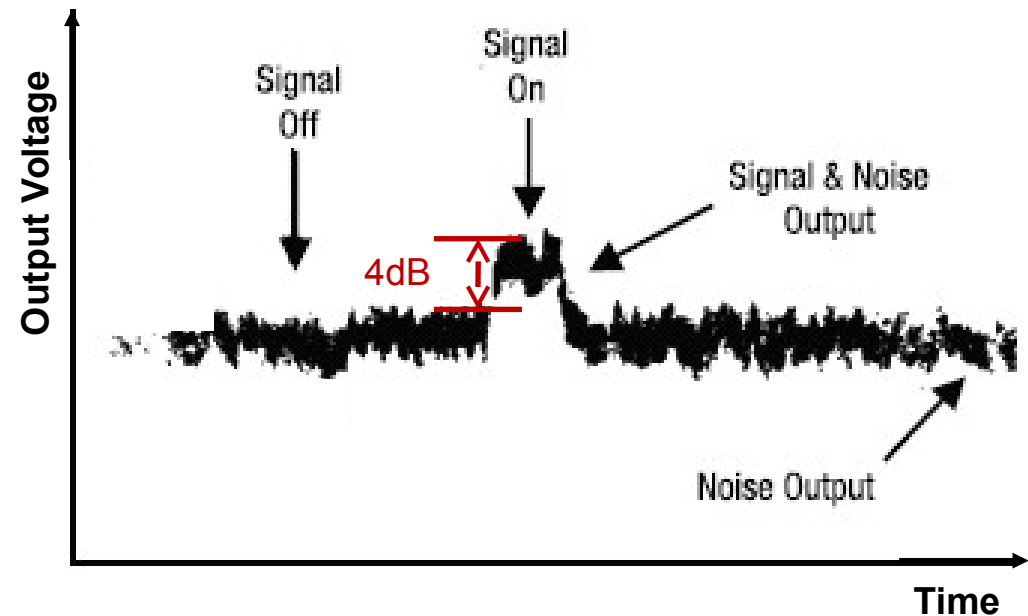
> -20 dBm: $V_{\text{Video}} \sim V_{\text{RF}}$



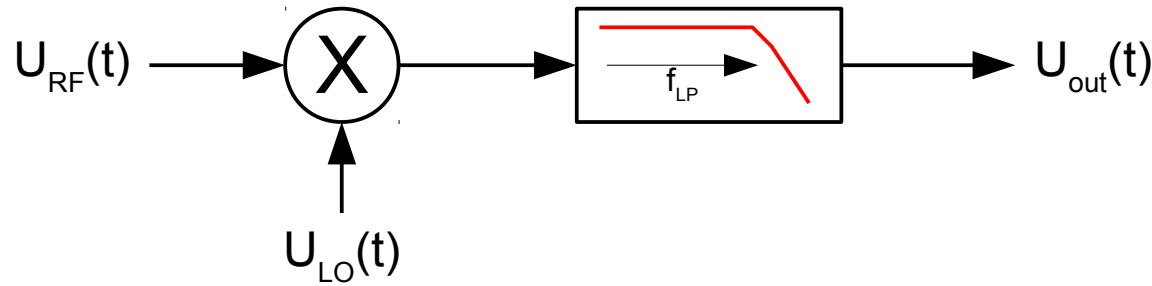
- The transition between the linear region and the square-law region is typically between -10 and -20 dBm RF power.
- Why does it matter ?
→ this is being used as and limits the fundamental property of RF mixers

RF Diode – Tangential Signal Sensitivity

- Due to the square-law characteristic we arrive at the thermal noise region already for moderate power levels (-50 to -60 dBm) and hence the V_{Video} disappears in the thermal noise
- This is described by the term
 - tangential signal sensitivity (TSS) where the detected signal is 4 dB over the thermal noise floor (Observation BW, usually 10 MHz)
- Passive RF detector are very robust but require that the carrier signal is above -60...-50 dBm ie. 250 mV



Classic Ideal RF (Down-)Mixer



$$\begin{aligned} U_{out}(t) &= LP(U_{RF}(t) \cdot U_{LO}(t)) \\ &= LP(U_1 \cdot \cos(2\pi f_{RF}) \cdot U_2 \sin(2\pi f_{LO})) \\ &= \frac{U_1 U_2}{2} \sin(2\pi(f_{RF} - f_{LO})) + \cancel{\frac{U_1 U_2}{2} \sin(2\pi(f_{RF} + f_{LO}))} \end{aligned}$$

removed by low-pass filter

- input/output port assignment is arbitrary but the low-pass is often implicit and defines the down-conversion port
 - RF: to be measured input
 - LO: local oscillator input (larger power, constant reference frequency)
 - Replacing the low- with a high-pass makes this an up-converter/mixer

Closer to Real-World Mixer

- From Shockley equation:

$$(\exp(x) - 1) = x + \frac{1}{2}x^2 + h.o.$$

- So if we sum two voltages prior to the diode

$$U_0 = \underbrace{(U_1 + U_2)}_{\text{removed by LP}} + \frac{1}{2} \underbrace{(U_1 + U_2)^2}_{\text{mostly removed by LP}} + \underbrace{h.o.}_{\text{mostly removed by LP}}$$

$$\frac{1}{2} \underbrace{U_1^2}_{\text{removed by LP}} + U_1 \cdot U_2 + \frac{1}{2} \underbrace{U_2^2}_{\text{removed by LP}}$$

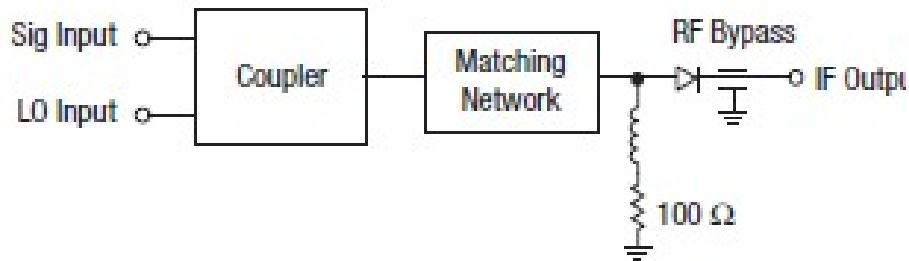
→ our homodyne RF diode detector is basically a mixer with the RF and LO port tight together ($U_1 = U_2$)

$$I(U) = I_S \left(\exp\left(\frac{eU}{mkT}\right) - 1 \right)$$

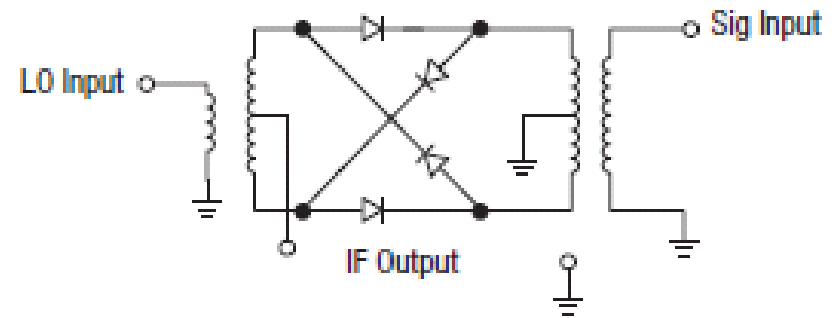
$$= I_S \left(\exp\left(\frac{U}{mU_T}\right) - 1 \right)$$

Real-World RF Diode Mixer Topologies

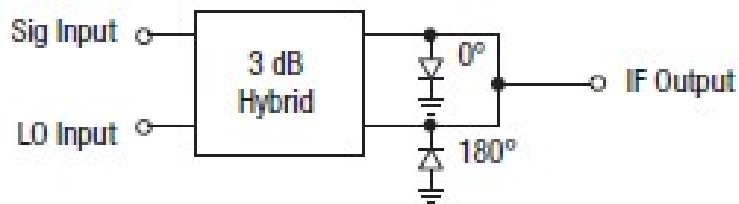
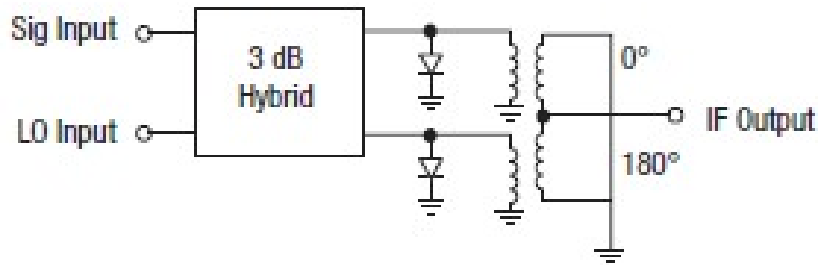
A. Single-Ended Mixer



C. Double-Balanced Mixer

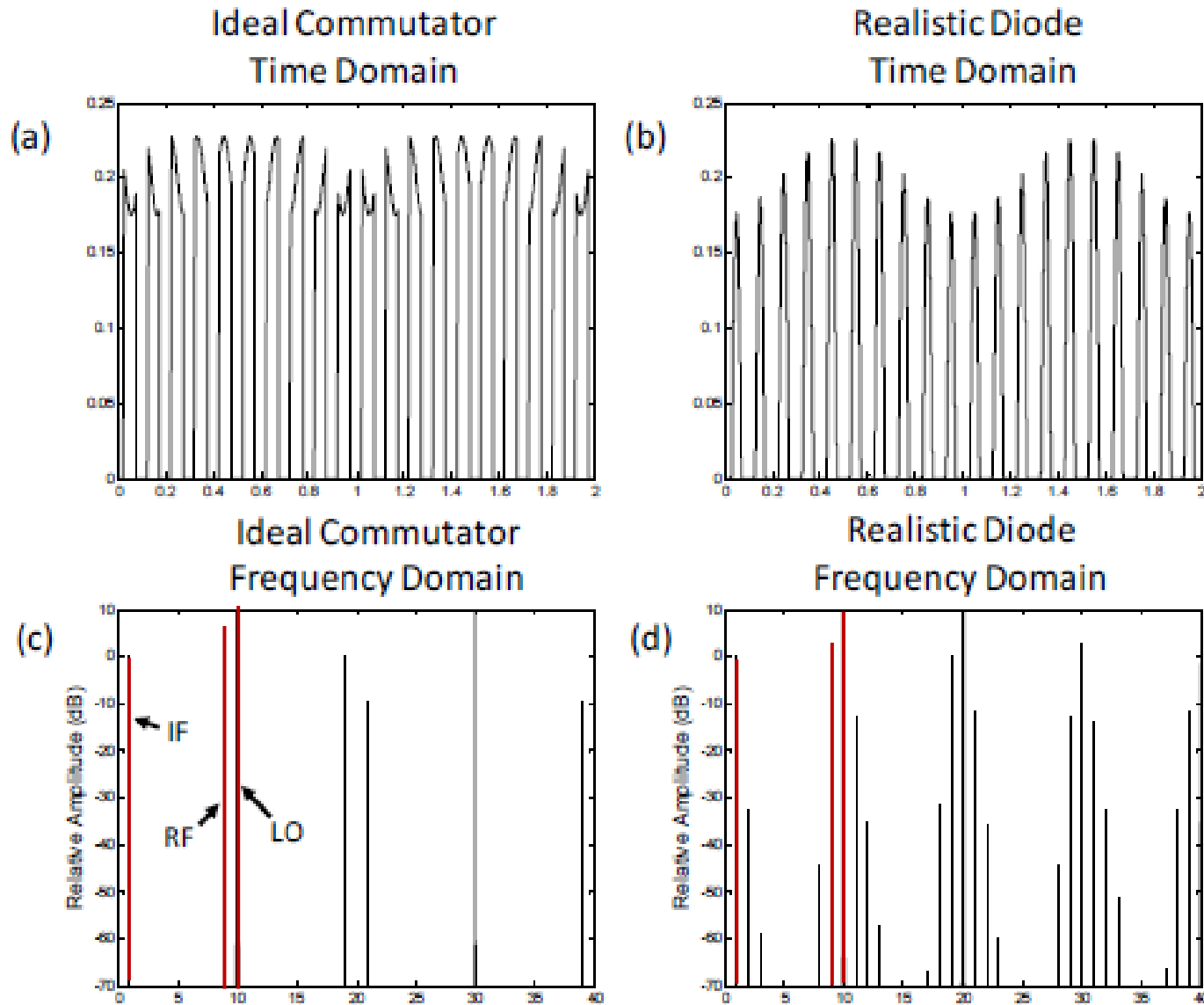


B. Balanced Mixers



A typical coaxial mixer (SMA connector)

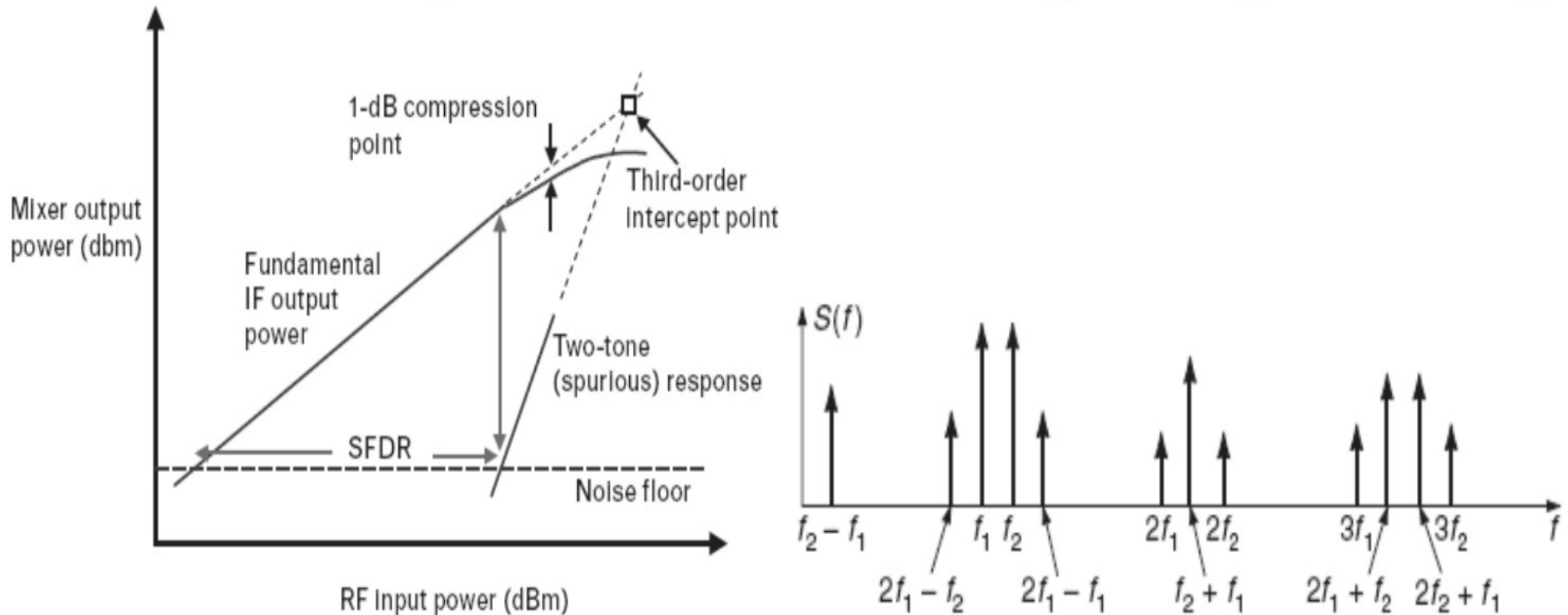
RF Mixer Time and Frequency Response



- Input signals here: LO = 10 MHz & RF = 8 MHz
 - Mixing products at 2 and 18 MHz are higher order terms

RF mixer – Dynamic range and IP3

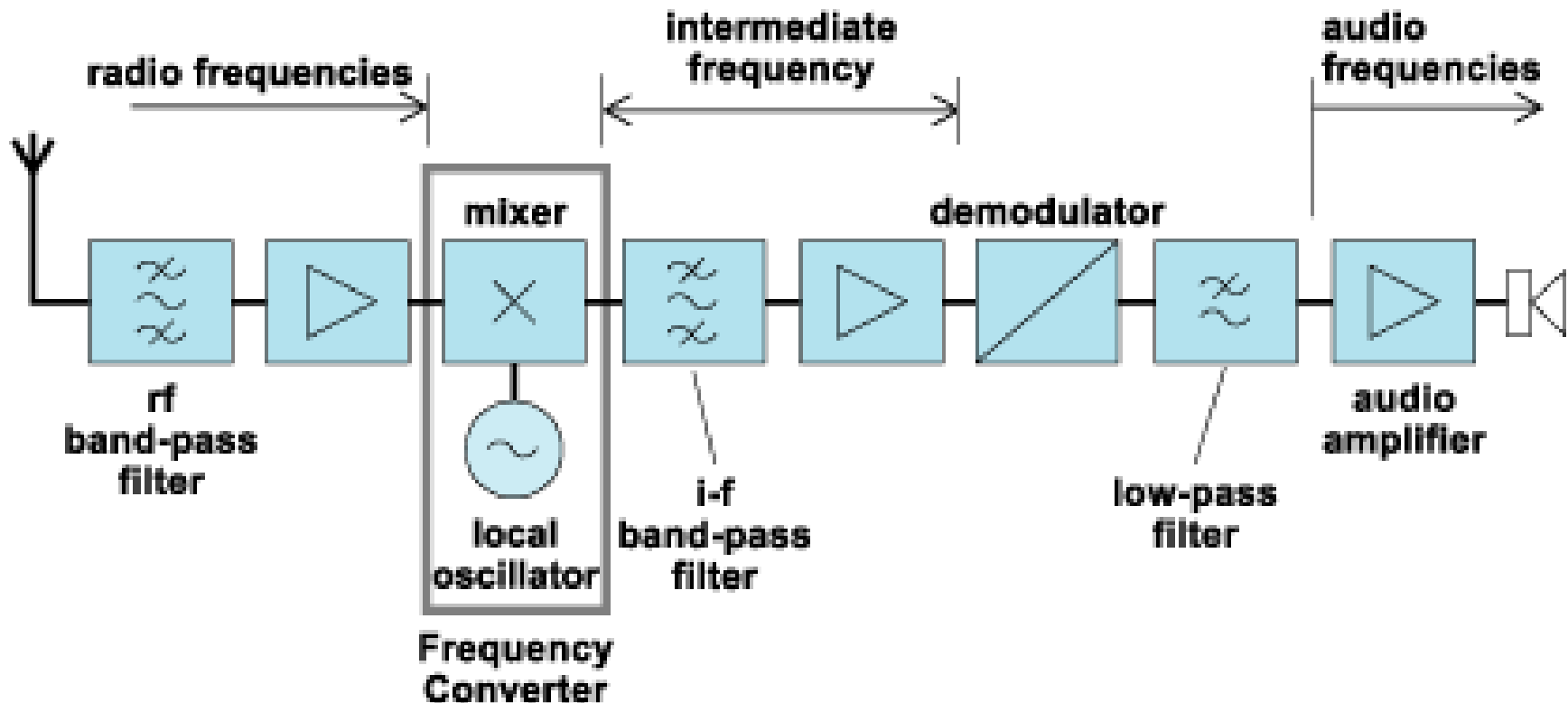
- 3rd-order Input Interception Point (IP3): RF input power at which the unwanted intermodulation products equal desired IF output.



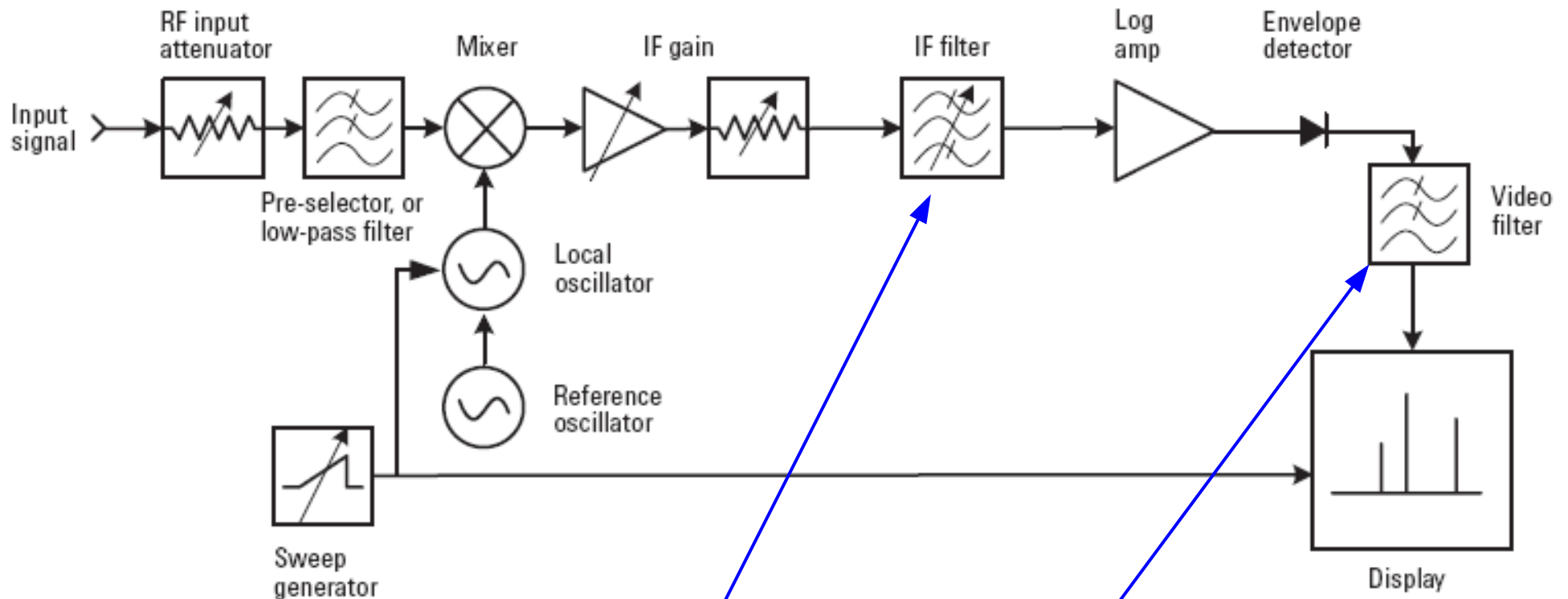
- N.B. this intersection point is usually extrapolated from lower power levels to not overload and damage of the DUT.

Super-Heterodyne Concept

- 'Super-' (*latin: over*) 'hetero-' (*greek: different*) -dyne (*greek: "power" or "force"*):
Superimposes a strong local-oscillator (LO) signal with a (usually weaker) radio-frequency (RF) signal
→ mixing produces intermediate (IF) frequency signal



Super-Heterodyne Application: Spectrum Analyser



The center frequency is fixed, but the bandwidth of the IF filter can be modified.

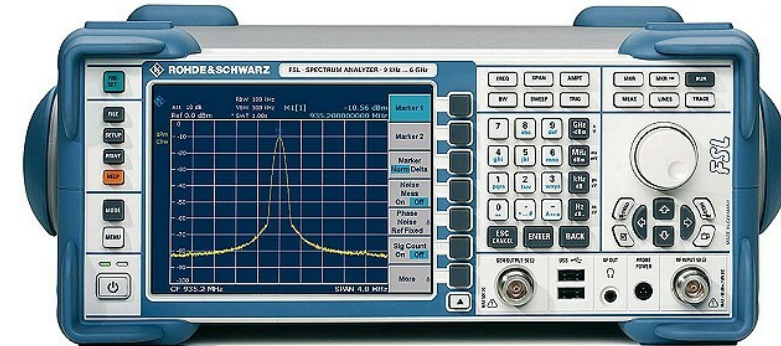
The video filter is a simple low-pass with variable bandwidth before the signal arrives to the vertical deflection plates of the cathode ray tube.

Agilent, 'Spectrum Analyzer Basics,'
Application Note 150, page 10 f.

Spectrum Analyser

- Spectrum Analyser (SA): observation in **time domain**

- application: observation of beam spectra or spectrum emitted from an antenna, etc.
- Classic version: sweeps through a given frequency range point by point with a very narrow bandwidth
- **Modern version: Dynamic signal analyzer (aka. Real-Time FFT/spectrum analyzer):**



Acquires signal in time domain by fast sampling with wider bandwidth (typ. 20 ... 200 MHz)

- Contrary to the SPA: non-repetitive signals and transients can be observed
- Further numerical treatment in digital signal processors (DSPs)
- Spectrum calculated using Fast Fourier Transform (FFT)
- Combines **features of a scope and a spectrum analyzer**: signals can be looked at directly in time domain or in frequency domain
- Application:
 - Observation of tune sidebands,
 - transient behaviour of a phase locked loop, etc.

Introduction to RF – Part I

- Aim: Learn how high-frequency signals are measured
- Part I – time-domain vs. frequency domain (RF Detectors and Mixers)
 - Bode plots, power and dB(m, c, uV) definitions,
 - AM vs. FM vs. PM modulation
 - RF (Schottky) Diodes → RF Detectors (homodyne detection)
 - RF Mixers (heterodyne detection)
 - Introduction to: oscilloscopes, spectrum analyser, vector network analyser
- Laboratory:
 - some simple simulations using QUCS – guided/students
 - in || lab measurement with generator + spectrum analyser
 - some simple simulations using QUCS – guided/student
 - “Play” with BPM mock-up
 - Repeat in || previous day experience now with some active elements