

Influence of Varying Tune Width on the Robustness of the LHC Tune PLL and its Application for Continuous Chromaticity Measurement A. Boccardi, M. Gasior, R. Jones, K.K. Kasinski, R.J. Steinhagen (CERN, Geneva)

# Abstract

Tune and chromaticity measurement is an integral part for safe and reliable LHC operation. Tight tolerances on the maximum transverse beam excursions allow oscillation amplitudes of less than 30 um. This leaves only a small margin for transverse beam and momentum excitations required for measuring tune and chromaticity. This contribution discusses a robust tune phase-locked-loop (PLL) operation in the presence of non-linearities and varying chromaticity. The loop design was tested at the SPS, using the LHC PLL prototype system. The system was also used to continuously measure tune width and chromaticity changes, using resonant transverse excitations of the tune side-slopes.

# **Parameter Stability Requirements**



Stability requirements on LHC tune and chromaticity are primarily driven by the ability to control particle loss. The lack of synchrotron radiation damping (hadrons) requires up to 12th order resonances to be avoided.

# **Expected Perturbations vs. Requirements:**

Sources: power supply drifts and ripples, hysteresis, ramp tracking errors, beam-beam, e-cloud, decay & snap-back, persistent currents, ...

--Ramp: max.  $\Delta Q' \approx 300$  units @  $\Delta Q'/\Delta t \approx 1.2$  units/s



200 400 600 800 1000 1200 1400 1600

« 0.01

± 1e-4

LHC collimation imposes tight constraints on the orbit/betatron oscillations:

$$\Delta z \leq 35 \,\mu m \rightarrow \frac{\Delta p}{p} < 10^{-1}$$

→ Classic Method: 
$$\Delta p/p > 10^{-3} \& \Delta Q_{res} \approx 10^{-3} \rightarrow \Delta Q'_{res} \sim 1$$

 $\Delta Q = Q' \frac{\Delta p}{m}$ 

• tough, still not established!

• R&D on alternative methods ongoing: cont. head-tail, side-exciter...

<b>X</b>				anie [3]	
	Orbit [σ]	Tune [0.5·f]	Chroma. [units]	Energy [Δp/p]	Coupling [c_]
Perturbations:	~ 1-2 (30 mm)	0.025 (0.06)	~ 70 (300)	± 1.5e-4	~0.01 (0.1)
Max. Drift Rate:	~ 25 µm/s	< 10 <sup>-3</sup> /s	< 1.3 s		
Pilot	-	± 0.1	+ 10 ??	-	-
Commissioning	± ~ 1	±0.015→0.003	> 0 ± 10	± 1e-4	« 0.03

## **Phase-Locked-Loop:**



# **PLL Controller Design Schematic:**

Control loop dynamics split into two parts:



2.Beam response:



 $\rightarrow$  open loop gain: K = const. (first order)

Open-Loop Transfer Function:  $G_{PLL}(s) \approx \tau s + 1$ (close-to-lock-condition approximation)

## Youla's Affine Parameterisation:

± 0.15

-300 0 200 400 600 800 1000 1200 1400 1600

Nominal

For any open-loop stable system, all stable closed loop controllers D(s) can be written as:

$$D(s) = \frac{Q(s)}{1 - Q(s)G(s)} \tag{1}$$

±0.003 / ±0.001 2 ± 1

Reduced closed-Loop response functions: reduced: classic:  $T_0(s) := \frac{y}{r} = \frac{DG}{1 + DG}$  $T_0(s) = QG$  $S_{d0}(s) := \frac{y}{\delta_d} = \frac{1}{1 + DG} \longrightarrow S_{d0}(s) = 1 - QG$  $S_{i0}(s) = (1 - QG)G$  $S_{i0}(s) := \frac{y}{s}$  $S_{u0}(s) = Q$ 

- FPGA based decoupled loop implementation:
- $\rightarrow$  phase-locked-loop  $\rightarrow$  tune
- controller task: adjust exciter frequency to match resonance condition  $\Delta \phi = \phi - 90^\circ = 0^\circ$
- $\rightarrow$  excitation amplitude loop  $\rightarrow$  limits max. excitation
- Further compensation for other non-beam related phase responses:
- constant lag (data processing, cables),
- analogue pre-filters, beam exciter response...



• Youla's Affine Parameterisation  $\rightarrow$  PI controller:

$$D(s) = K_P + K_i \frac{1}{s}$$
 with  $K_p = K_0 \frac{\tau}{\alpha} \wedge K_i = K_0 \frac{1}{\alpha}$ 

- optimal controller gains are coupled
- $-K_0$  fixed by effective tune width  $\rightarrow$  see right
- free parameter: closed-loop bandwidth  $1/\alpha$

## **FFT Acquisition without Tune PLL**



## **FFT Acquisition with Tune PLL**



$$S_{u0}(s) := \overline{\delta_d} = \overline{1 + DG}$$

• Using the following common ansatz (here: PLL example):

$$Q(s) = F_Q(s)G^i(s) = \frac{1}{\alpha s+1} \cdot \frac{\tau s+1}{K_0}$$

- $-F_{o}(s)$ : models the desired closed-loop response
- $G^{i}(s)$ : pseudo-inverse of the nominal plant G(s) • in case of non-lin. or unstable zeros e.g.:

 $G(s) = G_{lin}(s) \cdot G_{NL}(s) \cdot e^{-\lambda s} \cdot \dots \quad \rightarrow \quad G^{i}(s) = (G_{lin})^{-1}$ 

• (yields Smith predictor, anti-windup schemes, etc.)

• MP system: 
$$\rightarrow T_0(s) = F_Q(s) = \frac{1}{\alpha s + 1}$$

<sup>1</sup>D. C. Youla et al., "Modern Wiener-Hopf Design of Optimal Controllers", IEEE Trans. on Automatic Control, 1976, vol. 21-1,pp. 3-13 & 319-338 <sup>2</sup>R.J. Steinhagen, *"Feedbacks on Tune and Chromaticity"*, DIPAC'07, 2007

## **PLL Tune Trace Example:**





## Feedback Robustness ...and Betatron Coupling:

Strictly: PLL measures tune eigenmodes  $\beta$  - coupling may rotate these w.r.t. unperturbed tunes  $(q_x, q_y, \Delta = |q_y - q_y|)$ :

 $Q_{1,2} = \frac{1}{2} \left( q_x + q_y \pm \sqrt{\Delta^2 + |C^-|^2} \right)$ 

- Possible improvements:
- optimise tune working point (inc. tune-split), -vertical orbit stabilisation in lattice sextupoles ( $\rightarrow$  orbit FB!), active compensation and correction of coupling:



# ... in the Presence of Coupled Bunch Instabilities

- High-sensitivity tune pick-up (BBQ) enables PLL to operate within the transverse feedback "noise"
  - Pro: minimises inter-loop coupling effects
  - Con: no benefit from transverse damper suppression of e-cloud, impedance, beam-beam, etc. driven coupled bunch modes  $\rightarrow$  bunch selector



Two bunch model:  $regular \triangleright (\Sigma) \rightarrow output$ excitation  $\rightarrow$  G<sub>1</sub>(s)

coupled bunch

→ G<sub>2</sub>(s)

phase response

zero reference phase

2ΔQ ≈ 0.001 « 2Q

## ... in the Presence of Synchrotron Side-bands

Hilbert Transform relates amplitude to phase (MP System):  $\varphi(\omega) = Hilbert [ln | R(\omega)]$ 

 $\rightarrow$  PLL locks on the within the bandwidth largest peak







#### **Tune Feedback Robustness ...and Tune-width:**



- Design and optimal PLL parameters (tracking speed, etc.) depend - beside measurement noise - on the effective  $\Delta Q$ .



 $575E \pm 9$ 



#### Option I: gain scheduling

initial lock: open bandwidth to cover more than one side band (noise/chirp) • side-bands "cancel out", strongest resonance prevails once locked: reduce bandwidth for better stability/resolution

#### Option II: larger excitation bandwidth multiple exciter or broadband excitation (e.g. Tevatron/FNAL)

#### **Tune-width Dependence on Chromaticity:**







time [s]

$$\left(\frac{\Delta p}{p}\right)_{i, meas} \sim \underbrace{\sin(2\pi Q_s t + \phi_i)}_{= const} \rightarrow \left(\frac{\Delta p}{p}\right)_{i, meas} = const$$

$$\rightarrow \dot{\theta} \approx 2\pi \cdot \left[ Q_0 + Q' \cdot \frac{\Delta p}{p} \right] = const$$

## Summary:

The prototype test of the BBQ based tune PLL were very successful! Mutually exclusive modes of PLL operation:

Youla's affine parameterisation facilitates the trade-off selection and either: track tune changes with  $\Delta Q/\Delta t \approx 0.1/s$ simplifies the required dynamic adjustments due to varying tune width. achievable tune resolution  $\Delta Q_{res} \approx 10^{-4} \dots 10^{-5}$ 

BBQ based PLL showed to be very robust as long as bunch-to-bunch coupling was small will be addressed through selecting only single bunch Question is not: "Can we measure chromaticity?", but "Can we measure Q' with a given precision and minimal excitation?" -Requires studies of systematics with "slow" coasting beam to prove feasibility of LHC Q' baseline ( $\Delta Q'=1 \& \Delta p/p \ll 10-4$ )